



## Calibration of surface roughness standards

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# **Key Comparison EURAMET.L-K8.2013**

## **Calibration of surface roughness standards**

### **EURAMET project #1245**

## **Final report**

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Wabern, October 2015

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## 1 Document control

Version Draft B.1	Issued on April 2015.
Version Draft B.2	Issued on June 2015, comments participants taken in to account.
Version Draft B.3	Issued on August 2015, minor typos and comment in section 8.7.
Version Draft B.4	Issued on September 2015, minor editorial change.
Final report	Issued on October 2015, taking into account comments from CCL WG-MRA reviewers

## 2 Introduction

The metrological equivalence of national measurement standards and of calibration certificates issued by national metrology institutes is established by a set of key and supplementary comparisons chosen and organized by the Consultative Committees of the CIPM or by the regional metrology organizations in collaboration with the Consultative Committees.

At its meeting in October 2012, the EURAMET Technical Committee for length, EURAMET-TCL, decided upon a key comparison on the calibration of surface roughness standards, named EURAMET.L-K8.2013, with METAS as the pilot laboratory. The comparison was registered in January 2013, measurements were made between February 2013 and February 2015. The protocol followed the instructions of the preceding comparison EURAMET.L-K8 [1] as closely as possible.

## 3 Organization

### 3.1 Participants

**Table 1.** List of participant laboratories and their contacts.

Laboratory Code	Contact person, Laboratory	Phone, Fax, email
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### 3.2 Schedule

Details of the planned and actual schedules as well as date of receipt of results from the participants are shown in Table 2. The MRA states that the results should be sent within six weeks of completing the measurements.

**Table 2.** Schedule of the comparison.

RMO	Laboratory	Planned date of measurement	Actual date of measurement	Results received
EURAMET	METAS	Mar 2013	Feb 2013	11.03.2013
	DTU-CGM	Apr 2013	Apr 2013	14.08.2013
	MIKES	May 2013	May 2013	21.06.2013
	IPQ	Jun 2013	Jun 2013	08.08.2013
	BEV	July 2013	Jul 2013	06.09.2013
	SP	Aug 2013	Aug 2013	18.10.2013
	INRIM	Sep 2013	Sep 2013	18.04.2014
	LNE	Oct 2013	Oct 2013	11.04.2014
	CEM	Nov 2013	Nov 2013	04.09.2014
	GUM	Dec 2013	Dec 2013	31.01.2014
	METAS	Jan 2014	Jan 2014 (stability check)	13.01.2014
	DMDM	Feb 2013	Feb 2014	13.08.2014
	UME	Mar 2013	Mar 2014	27.05.2014
APMP	NIMT	Apr 2013	Apr 2014	06.06.2014
	NMC/A*STAR	May 2014	May 2014	03.10.2014
	CMS/ITRI	Jun 2014	Jun 2014	17.10.2014
AFRIMETS	NMISA	Jul 2014	Dec 2014	10.02.2015
SIM	INMETRO	Aug 2014	Aug 2014	08.12.2014
EURAMET	METAS	Sep 2014	Feb 2015 (stability check)	10.02.2015

The original schedule has been changed in the course of the comparison, mainly due to the requirement, that participants after January 2014 needed an ATA carnet and because NMISA was not ready with their equipment in the time slot originally allocated. There were no major transportation or customs problems, except import/export to and from Brazil, which took much more time. This didn't delay the comparison, since they were scheduled at the end of the circulation.

## 4 Artefacts

Five standards were circulated: one type A2, two type C1 and two type D1 according to ISO 5436-1 [2]. The standards were from different manufacturers and different materials. A plastic case (40 cm x 32 cm x 17 cm) containing 4 wooden boxes with the artefacts and the technical protocol was used for transportation (Figure 1).

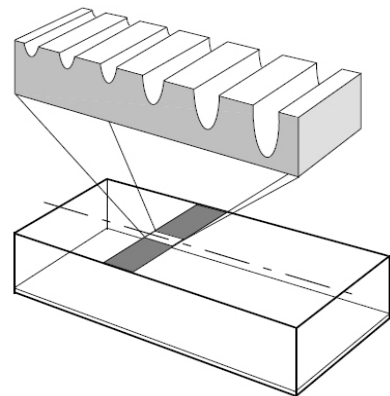


Figure 1. Transporting case.

### 4.1 Type A2 standard

**Depth measurement standard, KNT 2060/01, S/N 0589606**

Manufacturer: Halle, material: glass  
6 grooves with rounded bottoms,  
nominal values  $d$  0.33  $\mu\text{m}$  to 8.93  $\mu\text{m}$



### 4.2 Type C1 standard

**Spacing measurement standard, PGN 10, no 682060 5**

Manufacturer: Perthen, material: glass  
sine wave profile,  
nominal values  $R_a$  2.3  $\mu\text{m}$ ,  $R_{Sm}$  200  $\mu\text{m}$



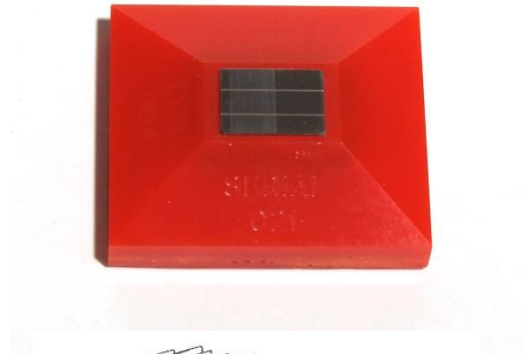


#### 4.3 Type D1 standard

##### **Roughness measurement standard, type 004, S/N 021**

Manufacturer: Rubert, material: electroformed metal,  
unidirectional irregular profile,  
nominal values  $Ra$  0.15  $\mu\text{m}$

Measurement area: Between the two marking lines.

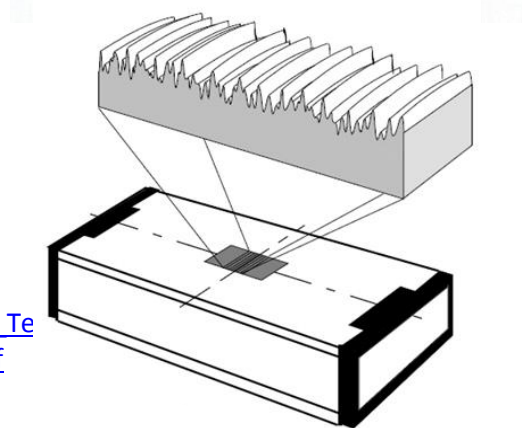


#### 4.4 Type D1 standard

##### **Roughness measurement standard, KNT 2070/03, S/N 0986**

Manufacturer: Halle, material: hard nickel plate  
unidirectional irregular profile,  
nominal values  $Ra$  0.06  $\mu\text{m}$

[http://www.halle-normale.de/pdf/2011/englisch/06\\_KNT-4058\\_Te\\_normale.de/pdf/2011/englisch/15\\_Ps-KNT-4070\\_BI\\_6-1\\_GB.pdf](http://www.halle-normale.de/pdf/2011/englisch/06_KNT-4058_Te_normale.de/pdf/2011/englisch/15_Ps-KNT-4070_BI_6-1_GB.pdf)



#### 4.5 Additional type C1 standard

##### **Spacing measurement standard, NIST SRM 2072, S/N 1015**

Manufacturer: NIST, material: steel  
sine wave profile,  
nominal values  $Ra$  1  $\mu\text{m}$ ,  $RSm$  100  $\mu\text{m}$



#### 4.6 Type F1 Reference data (softgauge)

Two softgauges in 7-bit ASCII character code (\*.smd format) according to ISO 5436-2 were included in a memory stick to investigate software algorithms independently of hardware variation:

*METAS\_Aperiodic.smd*: Aperiodic profile

*METAS\_Periodic.smd*: Periodic profile

The two data files correspond to primary profiles, i.e. after removal of form but before  $\lambda_s$  filtering. For laboratories not able to deal with the \*.smd format, also files in \*.prf format were available. The \*.prf format files were kindly transformed by LNE from the \*.smd format files.

## 5 Measuring instructions

### 5.1 Measurands

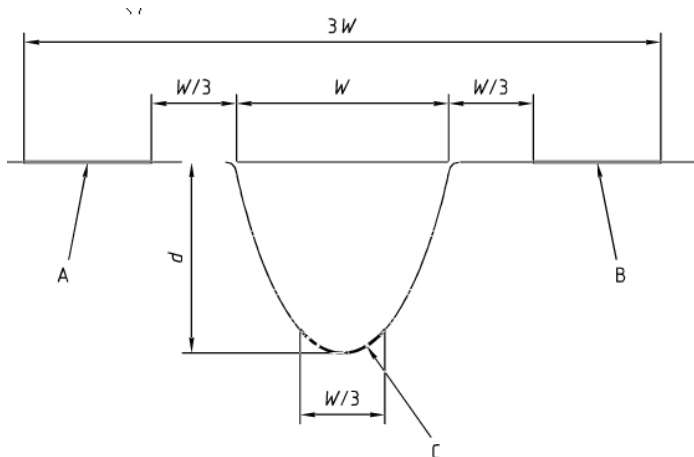
The following parameters were to be determined:

Artefact	Parameters	Relevant standards
<b>Type A2</b> KNT 2060/01	$d, Pt$	ISO 5436-1 [2] ISO 4287 [3]
<b>Type C1</b> PGN 10	$Ra, Rq, Rz, Rt, RSm$	ISO 5436-1 ISO 4287
<b>Type D1</b> S/N 021	$Ra, Rq, Rz, Rt$	ISO 5436-1 ISO 4287
<b>Type D1</b> KNT 2070/03	$Ra, Rq, Rz, Rt$	ISO 5436-1 ISO 4287
<b>Type C1</b> SRM 2072	$Ra, Rq, Rz, Rt, RSm$	ISO 5436-1 ISO 4287
<b>Type F1</b>	$Ra, Rq, Rz, Rt, Rsk, (RSm)$	ISO 5436-2 ISO 4287

For each parameter, its value and the observed standard deviation  $\sigma$  had to be reported.

### 5.2 Measurement and evaluation for type A2 artefact

A least squares mean line representing the upper level is drawn over the groove. A least squares circle is fitted through the centre third of the width of the groove. The depth  $d$  is evaluated from the line to the lowest point of the fitted circle (see Figure 2). The portions to be used for the evaluation are those shown at A, B and C in Figure 2. The average of five traces, evenly distributed over the measuring window, together with the standard deviation  $\sigma$  were to be reported.



**Figure 2.** Assessment of the depth measurement standard (ISO 5436-1).

Note, that the laboratories were also asked to determine  $Pt$  (see table in 5.1). However, since  $d$  is the standardized measurand for type A2 standards according to ISO 5436-1 and all laboratories were able to determine  $d$ , the  $Pt$  results are not reported here because they would provide essentially redundant information. They were, however, included in the results spreadsheet distributed to the participants.

### 5.3 Measurement conditions for type C1 and D1 artefacts

The average of twelve traces, evenly distributed over the measuring window, together with the standard deviation  $\sigma$  were to be reported. A Gaussian filter according to ISO 16610-21:2011 had to be applied for evaluating the  $R$  parameters.

Standard	Evaluation length (mm)	$\lambda_c$ ( $\mu\text{m}$ )	$\lambda_s$ ( $\mu\text{m}$ )	Measuring force (mN)	Sampling spacing ( $\mu\text{m}$ )	Tip radius ( $\mu\text{m}$ )
Type C1 PGN 10	4.00	800	2.5	< 1	$\leq 0.5$	2
Type D1 S/N 021	4.00	800	2.5	< 1	$\leq 0.5$	2
Type D1 KNT 2070/03	1.25	250	2.5	< 1	$\leq 0.5$	2
Type C1 SRM 2072	4.00	800	2.5	< 1	$\leq 0.5$	2

### 5.4 Evaluation of type F1 reference data

The following evaluation parameters were to be respected:

Standard	File name	Evaluation length (mm)	$\lambda_c$ ( $\mu\text{m}$ )	$\lambda_s$ ( $\mu\text{m}$ )	Parameters
F1 aperiodic	METAS_Aperiodic.smd	1.25	250	2.5	$Ra, Rq, Rz, Rt, Rsk$
F1 periodic	METAS_Periodic.smd	4.00	800	2.5	$Ra, Rq, Rz, Rt, Rsk, RSm$

The total profile length is 7 cutoff lengths ( $7 \lambda_c$ ). The evaluation length  $l_n$  was the five central sampling length  $l_r = \lambda_c$ , thus removing one cutoff length on each side in order to avoid end effects.

## 6 Stability of artefacts

### 6.1 Stability measurements

METAS measured the samples in February 2013, in January 2014 and in February 2015, i.e. at the beginning, in the middle and at the end of the comparison. Note that only the first result in February 2013 accounts for the key comparison, the other two were to monitor the stability of the samples. For simplicity, the evaluation of these measurement data was done in the same way as for the participant's results, i.e. the deviation from the weighted mean and the  $E_n$  values were calculated for each parameter and each standard.

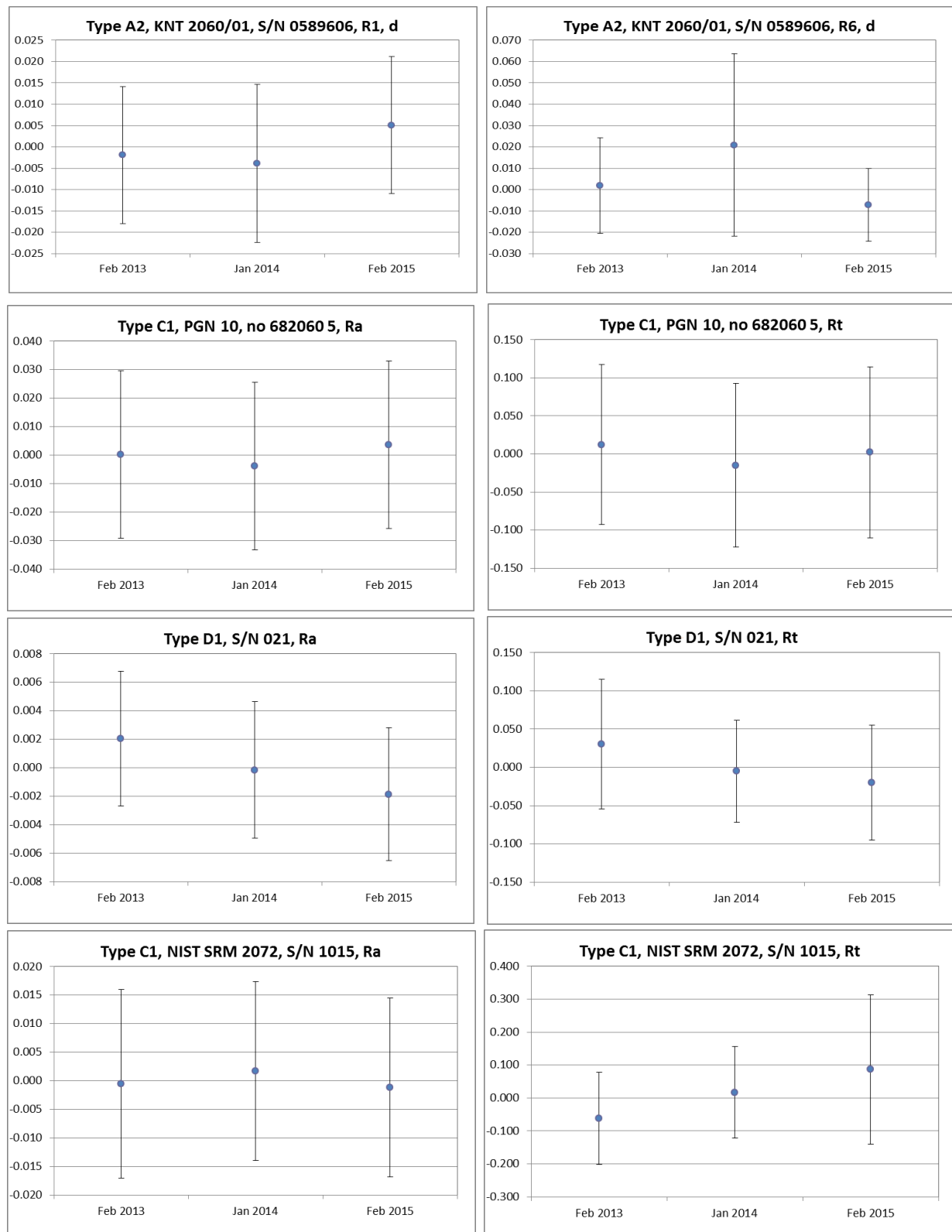
Table 3 shows the results of the stability measurements carried out by the pilot laboratory, where the "reference value"  $x_{\text{ref}}$  is the weighted mean of the three results  $x_i$ . All  $E_n$  values are smaller than 0.5, which can be interpreted that there is no significant change within the uncertainty.

**Table 3.** Results of stability measurements by the pilot laboratory.

Parameter	Period	$x_i / \mu\text{m}$	$u_i / \mu\text{m}$	$(x_i - x_{\text{ref}}) / \mu\text{m}$	$U(x_i - x_{\text{ref}}) / \mu\text{m}$	$E_n$
<b>Type A2, KNT 2060/01, S/N 0589606</b>						
R1, $d$	Feb 2013	0.317	0.010	-0.002	0.016	0.12
	Jan 2014	0.315	0.011	-0.004	0.019	0.21
	Feb 2015	0.324	0.010	0.005	0.016	0.32
R2, $d$	Feb 2013	0.405	0.011	-0.001	0.017	0.05
	Jan 2014	0.407	0.011	0.001	0.017	0.07
	Feb 2015	0.405	0.016	-0.001	0.029	0.03
R3, $d$	Feb 2013	1.343	0.011	0.001	0.019	0.06
	Jan 2014	1.344	0.010	0.002	0.016	0.13
	Feb 2015	1.339	0.010	-0.003	0.016	0.18
R4, $d$	Feb 2013	2.713	0.011	-0.003	0.018	0.17
	Jan 2014	2.723	0.012	0.007	0.020	0.35
	Feb 2015	2.713	0.011	-0.003	0.018	0.17
R5, $d$	Feb 2013	5.520	0.011	-0.004	0.018	0.22
	Jan 2014	5.533	0.012	0.009	0.020	0.45
	Feb 2015	5.520	0.011	-0.004	0.018	0.22
R6, $d$	Feb 2013	8.915	0.014	0.002	0.022	0.09
	Jan 2014	8.934	0.023	0.021	0.043	0.49
	Feb 2015	8.906	0.012	-0.007	0.017	0.42
<b>Type C1, PGN 10, no 682060 5</b>						
Ra	Feb 2013	2.372	0.018	0.000	0.029	0.01
	Jan 2014	2.368	0.018	-0.004	0.029	0.13
	Feb 2015	2.375	0.018	0.004	0.029	0.13
Rq	Feb 2013	2.660	0.020	0.002	0.032	0.05
	Jan 2014	2.654	0.021	-0.005	0.035	0.14
	Feb 2015	2.662	0.021	0.003	0.035	0.09
Rz	Feb 2013	7.705	0.063	0.021	0.102	0.21
	Jan 2014	7.663	0.063	-0.020	0.102	0.20
	Feb 2015	7.682	0.067	-0.001	0.112	0.01
Rt	Feb 2013	7.764	0.065	0.012	0.105	0.12
	Jan 2014	7.737	0.066	-0.015	0.108	0.14
	Feb 2015	7.754	0.068	0.002	0.112	0.02
RSm	Feb 2013	199.930	0.067	-0.055	0.109	0.50
	Jan 2014	199.990	0.067	0.005	0.109	0.05
	Feb 2015	200.033	0.067	0.049	0.109	0.45

Parameter	Period	$x_i / \mu\text{m}$	$u_i / \mu\text{m}$	$(x_i - x_{\text{ref}}) / \mu\text{m}$	$U(x_i - x_{\text{ref}}) / \mu\text{m}$	$E_n$
<b>Type D1, S/N 021</b>						
Ra	Feb 2013	0.126	0.003	0.002	0.005	0.43
	Jan 2014	0.124	0.003	0.000	0.005	0.03
	Feb 2015	0.122	0.003	-0.002	0.005	0.40
Rq	Feb 2013	0.159	0.003	0.002	0.005	0.31
	Jan 2014	0.157	0.003	0.000	0.005	0.04
	Feb 2015	0.155	0.003	-0.002	0.005	0.36
Rz	Feb 2013	1.056	0.039	0.009	0.064	0.14
	Jan 2014	1.060	0.038	0.013	0.062	0.20
	Feb 2015	1.027	0.037	-0.020	0.060	0.33
Rt	Feb 2013	1.220	0.050	0.030	0.085	0.36
	Jan 2014	1.184	0.043	-0.005	0.067	0.08
	Feb 2015	1.170	0.046	-0.020	0.075	0.26
<b>Type D1, KNT 2070/03, S/N 0986</b>						
Ra	Feb 2013	0.060	0.002	0.000	0.004	0.03
	Jan 2014	0.060	0.002	0.000	0.004	0.03
	Feb 2015	0.060	0.002	0.000	0.004	0.00
Rq	Feb 2013	0.075	0.002	0.000	0.004	0.01
	Jan 2014	0.075	0.002	0.000	0.004	0.02
	Feb 2015	0.075	0.002	0.000	0.004	0.01
Rz	Feb 2013	0.326	0.021	0.000	0.034	0.00
	Jan 2014	0.324	0.021	-0.002	0.034	0.06
	Feb 2015	0.328	0.021	0.002	0.034	0.06
Rt	Feb 2013	0.442	0.023	-0.001	0.038	0.04
	Jan 2014	0.444	0.023	0.001	0.037	0.02
	Feb 2015	0.444	0.023	0.001	0.037	0.02
<b>Type C1, NIST SRM 2072, S/N 1015</b>						
Ra	Feb 2013	1.010	0.010	-0.001	0.017	0.03
	Jan 2014	1.012	0.010	0.002	0.016	0.11
	Feb 2015	1.009	0.010	-0.001	0.016	0.08
Rq	Feb 2013	1.120	0.011	-0.001	0.018	0.06
	Jan 2014	1.124	0.011	0.003	0.017	0.15
	Feb 2015	1.120	0.011	-0.002	0.017	0.09
Rz	Feb 2013	3.350	0.090	-0.040	0.147	0.27
	Jan 2014	3.418	0.089	0.028	0.144	0.20
	Feb 2015	3.400	0.090	0.011	0.148	0.07
Rt	Feb 2013	3.370	0.090	-0.061	0.140	0.44
	Jan 2014	3.448	0.090	0.017	0.139	0.12
	Feb 2015	3.518	0.126	0.087	0.226	0.38
RSm	Feb 2013	101.658	0.063	0.044	0.097	0.45
	Jan 2014	101.600	0.060	-0.014	0.090	0.16
	Feb 2015	101.540	0.101	-0.074	0.186	0.40

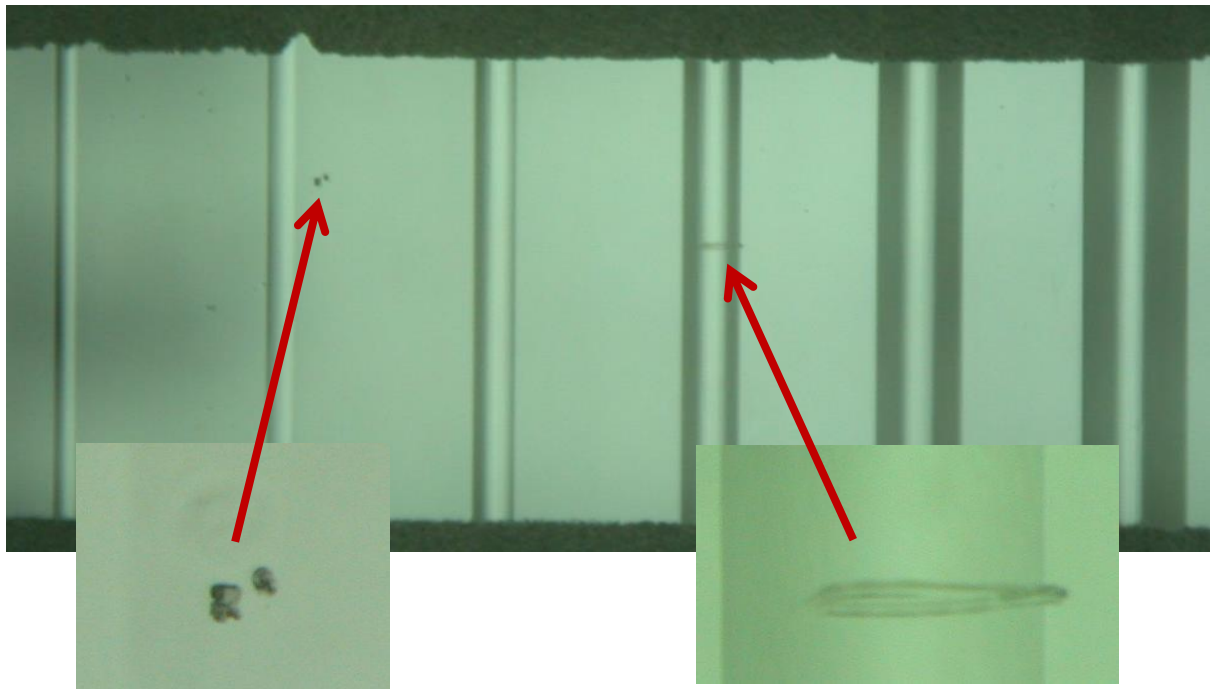
For some of the parameters, the stability results are also represented graphically in Figure 3.



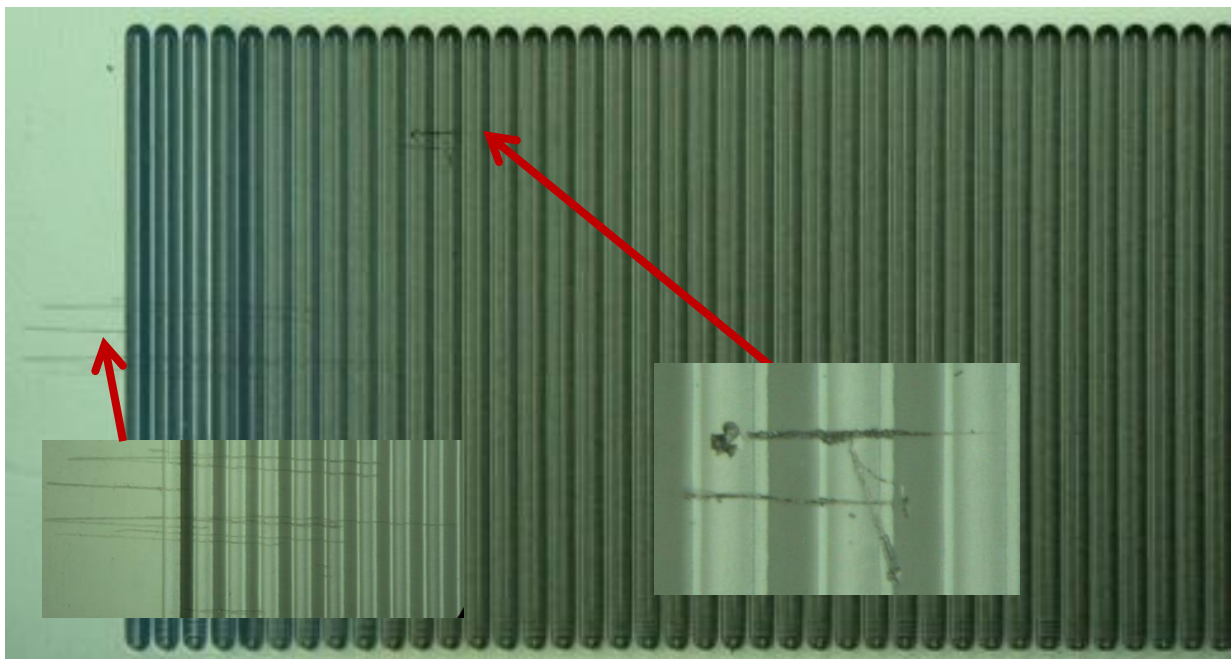
**Figure 3.** Stability measurements for selected standards and parameters (uncertainty bars for  $k = 2$ ).

## 6.2 Condition of artefacts at the end of comparison

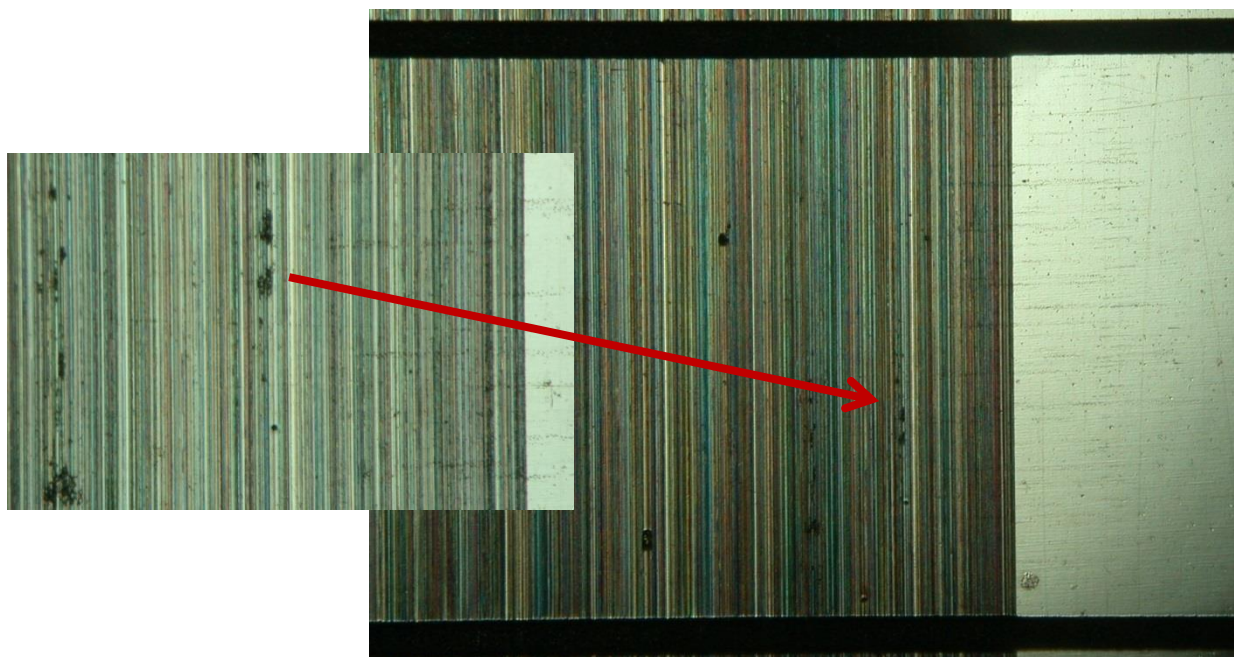
Several defects and damages on the standards were reported by the participants, already at an early stage of the comparison. The pilot did not try to identify the date and place, where the damages occurred. However, since the participants were free to choose the exact location of the measured profiles on the artefacts, there was always the possibility to choose a place more or less free of defects. In case a measurement was influenced by a surface defect, this accounts for the standard deviation and is therefore part of the measurement uncertainty. In Figure 4 to Figure 8, the status of the standards is documented as observed by the pilot at the end of the comparison.



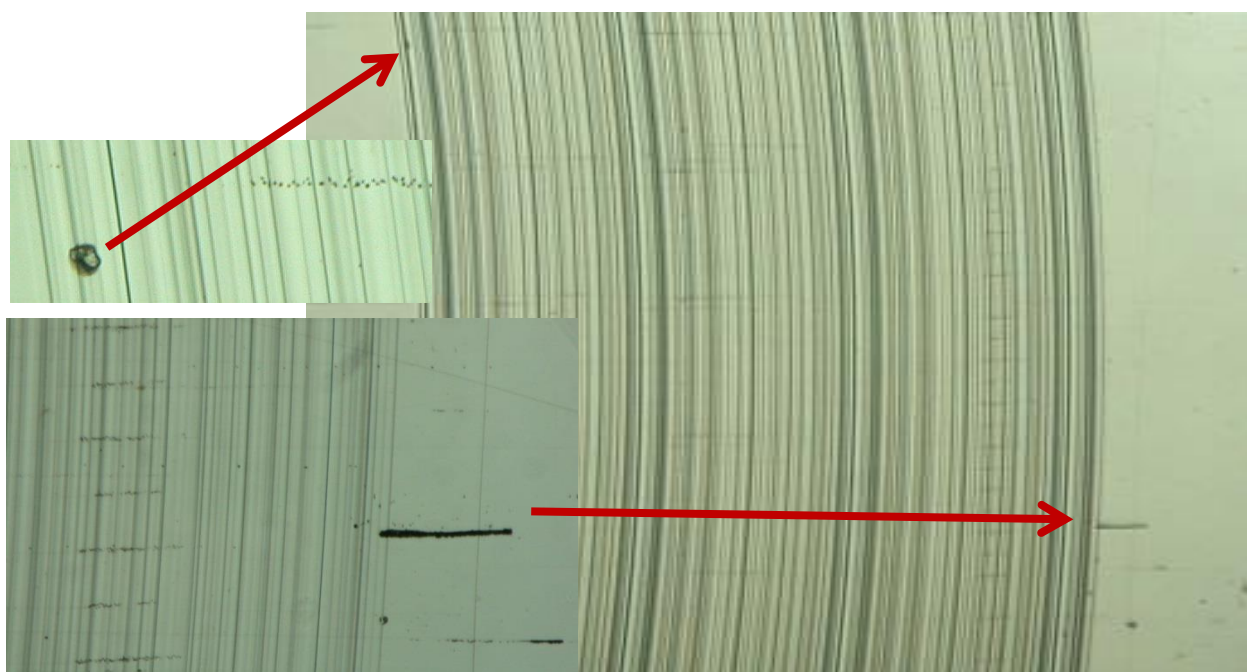
**Figure 4.** Defects on the standard Halle A2 KNT 2060/01.



**Figure 5.** Defects on the standard Perthen C1 PGN 10.

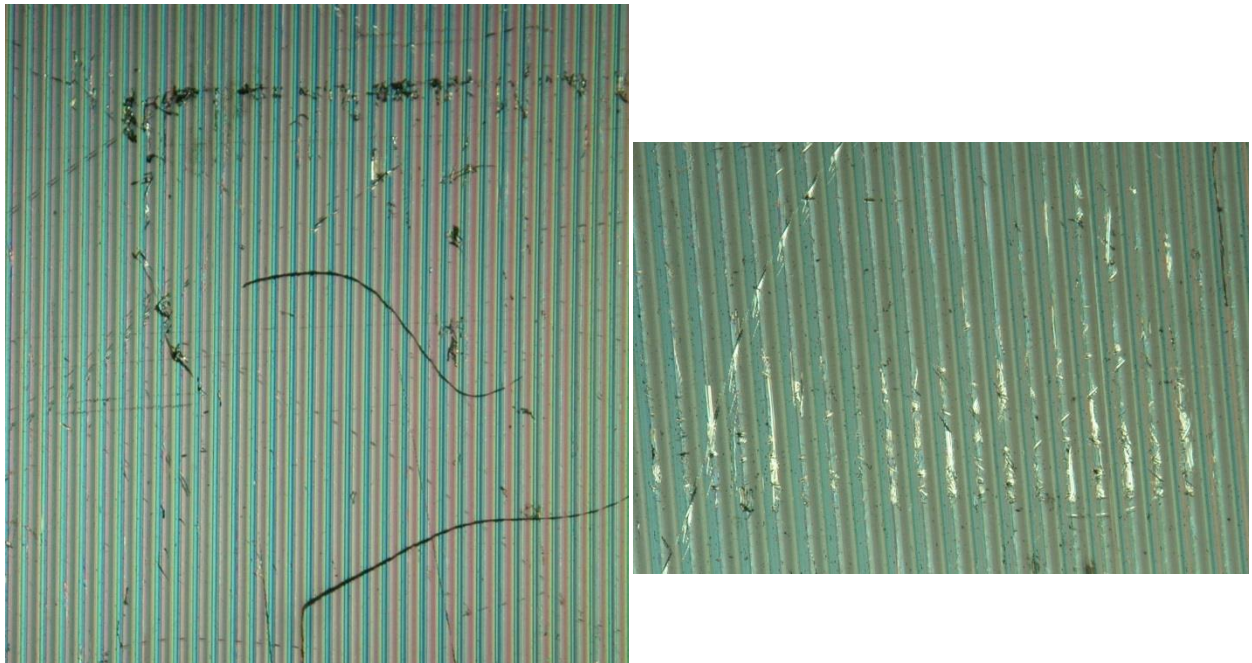


**Figure 6.** Defects on the standard Rubert D1 SN021.



**Figure 7.** Defects on the standard Halle D1 KNT2070/03.





**Figure 8.** Two defects on the standard NIST C1 SRM 2072.

### **6.3 Description of the damages observed at the end of the comparison**

#### Halle A2 KNT 2060/01

- Scratch on groove R4 (due to a stylus?)

#### Perthen C1 PGN 10

- Stylus scratches left in the middle
- Damage left above

#### Rubert D1 SN021

- Several stylus scratches
- 3 black spots
- dirty grooves

#### Halle D1 KNT2070/03

- Stylus scratches all over the surface
- Deep scratch on right side
- Round damage left above

#### NIST C1 SRM 2072

- Numerous damages and scratches all over the surface.

Note: The pilot did not photographically document the status of the surfaces at the beginning of the comparison. Some minor defects might have been present before the circulation of the standards.

## 7 Results

### 7.1 Results and standard uncertainties as reported by participants

The results had to be reported by the participants on Word forms in tables such as Table 4. These were all copied in an Excel spreadsheet *EURAMET.L-K8.2013-evaluation.xlsx*, which served as Draft A report of this comparison. The spread sheet allows for the evaluation of the reference values according to section 8.1 of this report, for the determination of the largest consistent subset and the degrees of equivalence. The results as they were reported by the participants are shown in section 8.2.

**Table 4.** Format of how the results had to be reported by the participants.

Parameter	Value (μm)	σ (μm)	u <sub>c</sub> (nm)	v <sub>eff</sub>
Ra				
Rq				
Rz				
Rt				
RSm				

σ: standard deviation

u<sub>c</sub>: standard uncertainty

v<sub>eff</sub>: number of effective degrees of freedom (if estimated)

## 8 Analysis of the measurement results

### 8.1 Calculation of the KCRV and of the Degrees of Equivalence

The Key Comparison Reference Values KCRV were calculated for each measurand using the weighted mean. To each result  $x_i$  a normalised weight  $w_i$  was attributed, given by:

$$w_i = C \cdot \frac{1}{[u(x_i)]^2} \quad (1)$$

where the normalising factor,  $C$ , is given by:

$$C = \frac{1}{\sum_{i=1}^I \left( \frac{1}{u(x_i)} \right)^2} \quad (2)$$

The weighted mean  $\bar{x}_w$  is given by:

$$\bar{x}_w = \sum_{i=1}^I w_i \cdot x_i \quad (3)$$

and the uncertainty of the weighted mean is calculated by:

$$u(\bar{x}_w) = \sqrt{\frac{1}{\sum_{i=1}^I \left( \frac{1}{u(x_i)} \right)^2}} = \sqrt{C} \quad (4)$$

After deriving the weighted mean and its associated standard uncertainty, the deviation of each laboratory's result from the weighted mean is determined simply as  $x_i - \bar{x}_w$ . The uncertainty of this deviation is calculated as a combination of the uncertainties of the result,  $u(x_i)$ , and the uncertainty of the weighted mean  $u(\bar{x}_w)$ . The uncertainty of the deviation from the weighted mean is given by

$$u(x_i - \bar{x}_w) = \sqrt{[u(x_i)]^2 - [u(\bar{x}_w)]^2} . \quad (5)$$

For the determination of the key comparison reference value KCRV, statistical consistency of the results contributing to the KCRV is required. A check for statistical consistency of the results with their associated uncertainties can be made by the so-called Birge ratio  $R_B$  which compares the observed spread of the results with the spread expected from the individual reported uncertainties.

The application of least squares algorithms and the  $\chi^2$ -test leads to the Birge ratio

$$R_B = \frac{u_{ext}(\bar{x}_w)}{u(\bar{x}_w)} , \quad (6)$$

where  $u_{ext}(\bar{x}_w)$  is the external standard deviation

$$u_{ext}(\bar{x}_w) = \sqrt{\frac{1}{(I-1)} \cdot \frac{\sum_{i=1}^I w_i (x_i - \bar{x}_w)^2}{\sum_{i=1}^I w_i}} . \quad (7)$$

The Birge ratio has an expectation value of  $R_B = 1$ , when considering standard uncertainties. For a coverage factor of  $k = 2$ , the expectation value is increased and the data in a comparison are consistent provided that

$$R_B < \sqrt{1 + \sqrt{8/(I-1)}} , \quad (8)$$

where  $I$  is the number of laboratories.

For each laboratory's result the  $E_n$  value is calculated, where  $E_n$  is defined as the ratio of the deviation from the weighted mean, divided by the expanded uncertainty of this deviation:

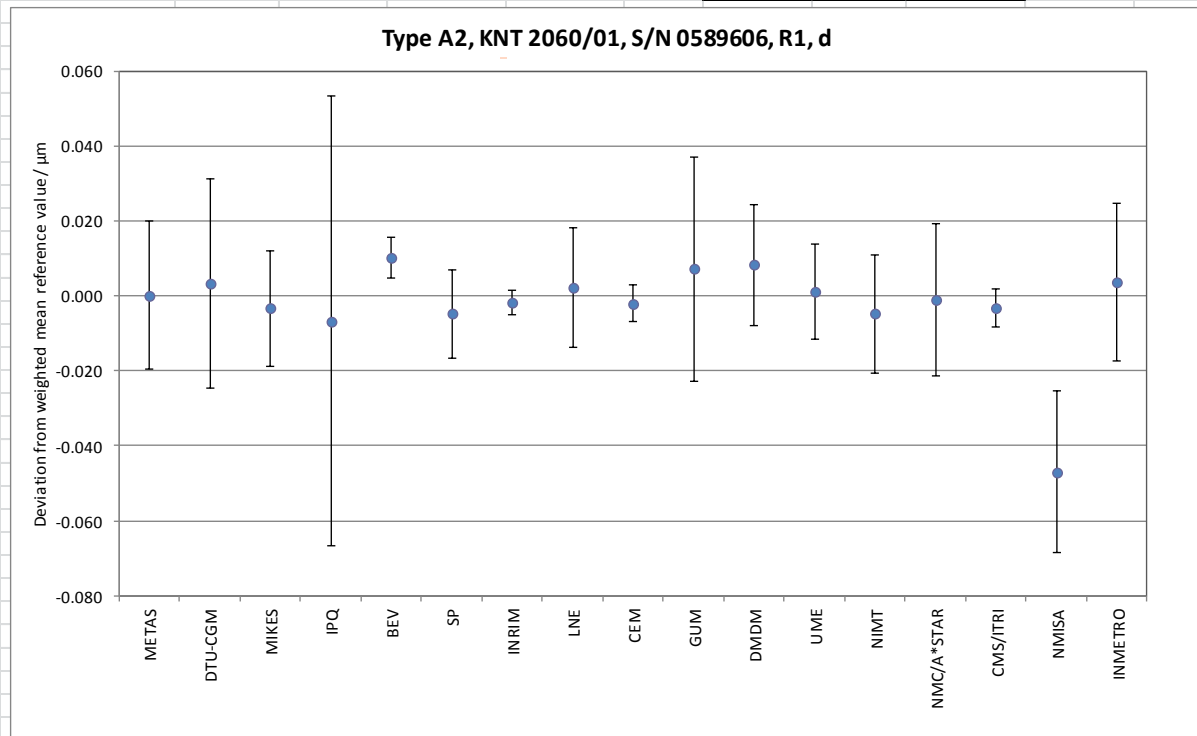
$$E_n = \frac{|x_i - \bar{x}_w|}{\sqrt{[U(x_i)]^2 - [U(\bar{x}_w)]^2}} . \quad (9)$$

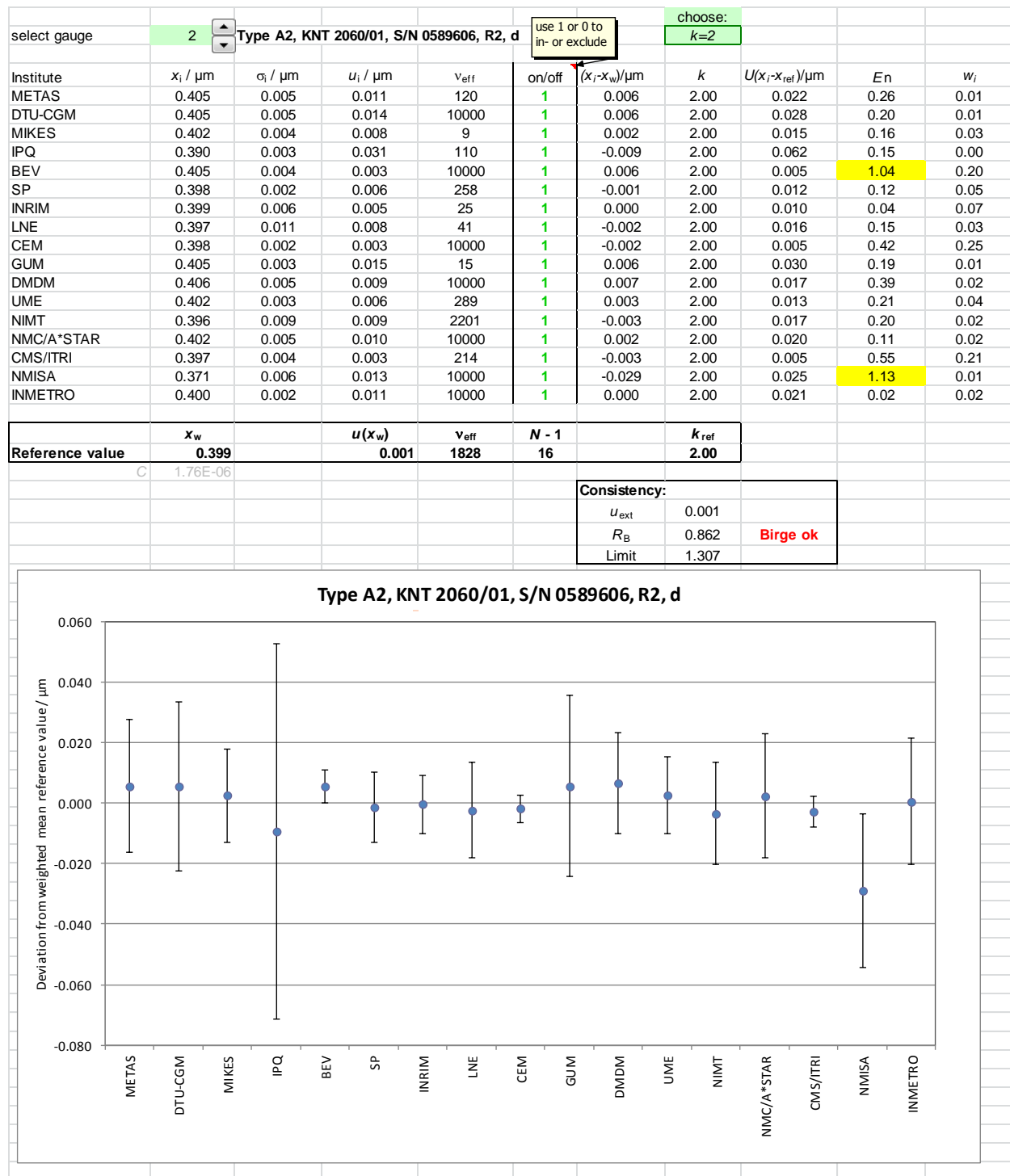
If statistical consistency according to equation (8) is not given, the result with the largest  $E_n$  is identified and excluded from the reference value and  $R_B$  is calculated again. This process of excluding the result with the largest  $E_n$  from contributing to the weighted mean is iterated until statistical consistency is reached.

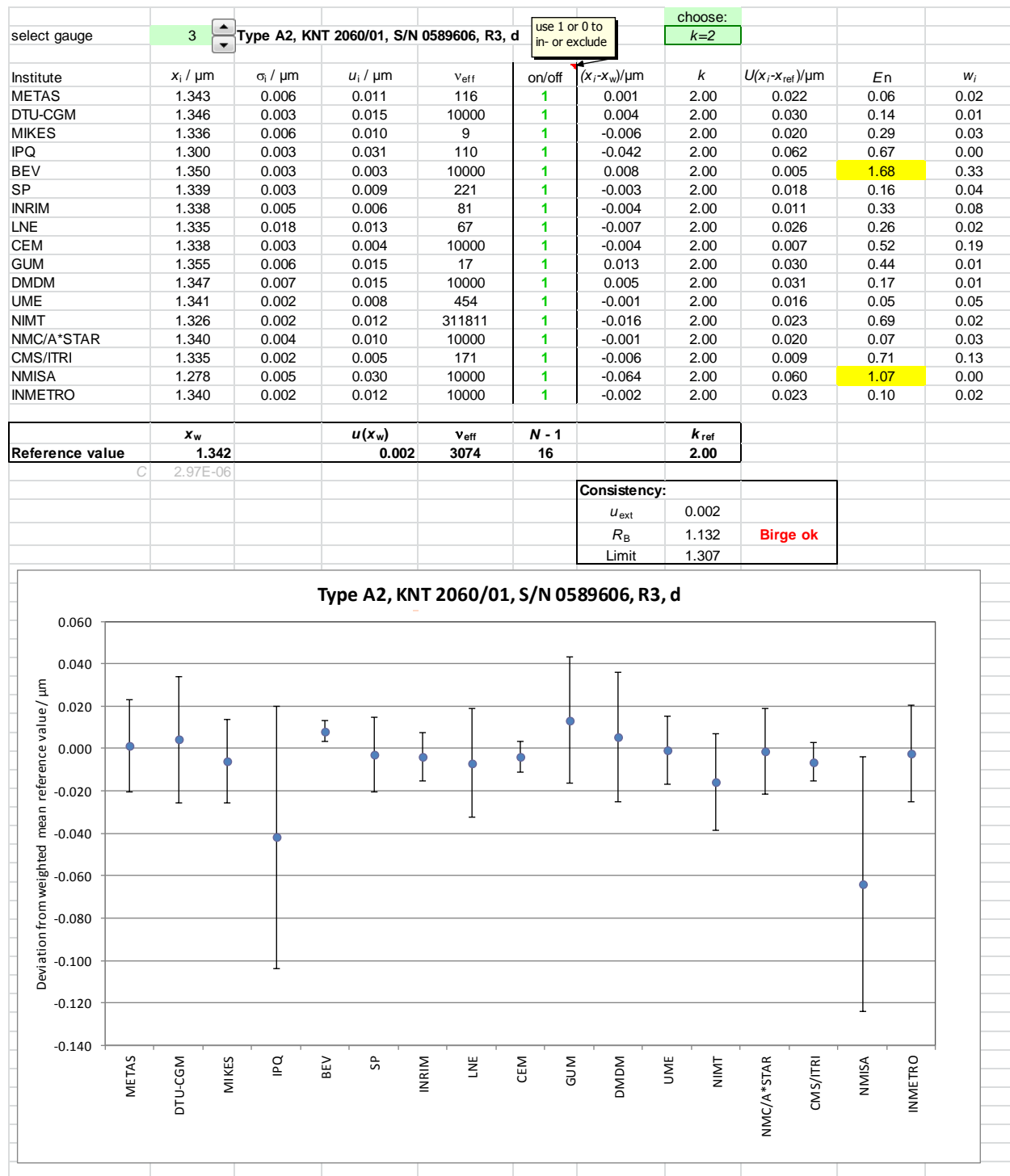
Because inconsistent results are no longer correlated with the weighted mean, when calculating their  $E_n$  value a positive sign is used in equation (5) and consequently in the denominator of equation (9):

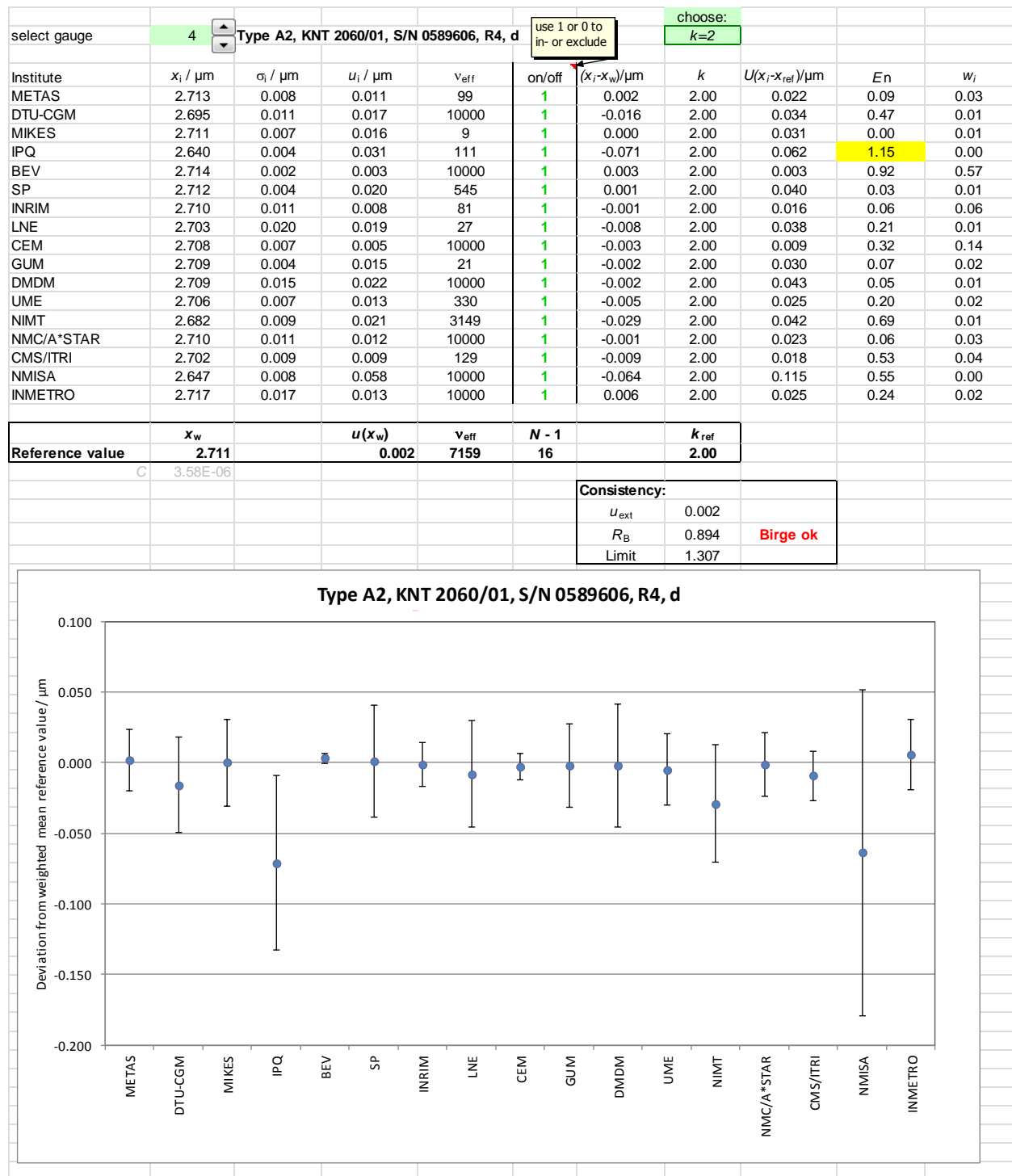
$$E_n = \frac{|x_i - \bar{x}_w|}{\sqrt{[U(x_i)]^2 + [U(\bar{x}_w)]^2}} \text{ for results excluded from the KCRV.} \quad (10)$$

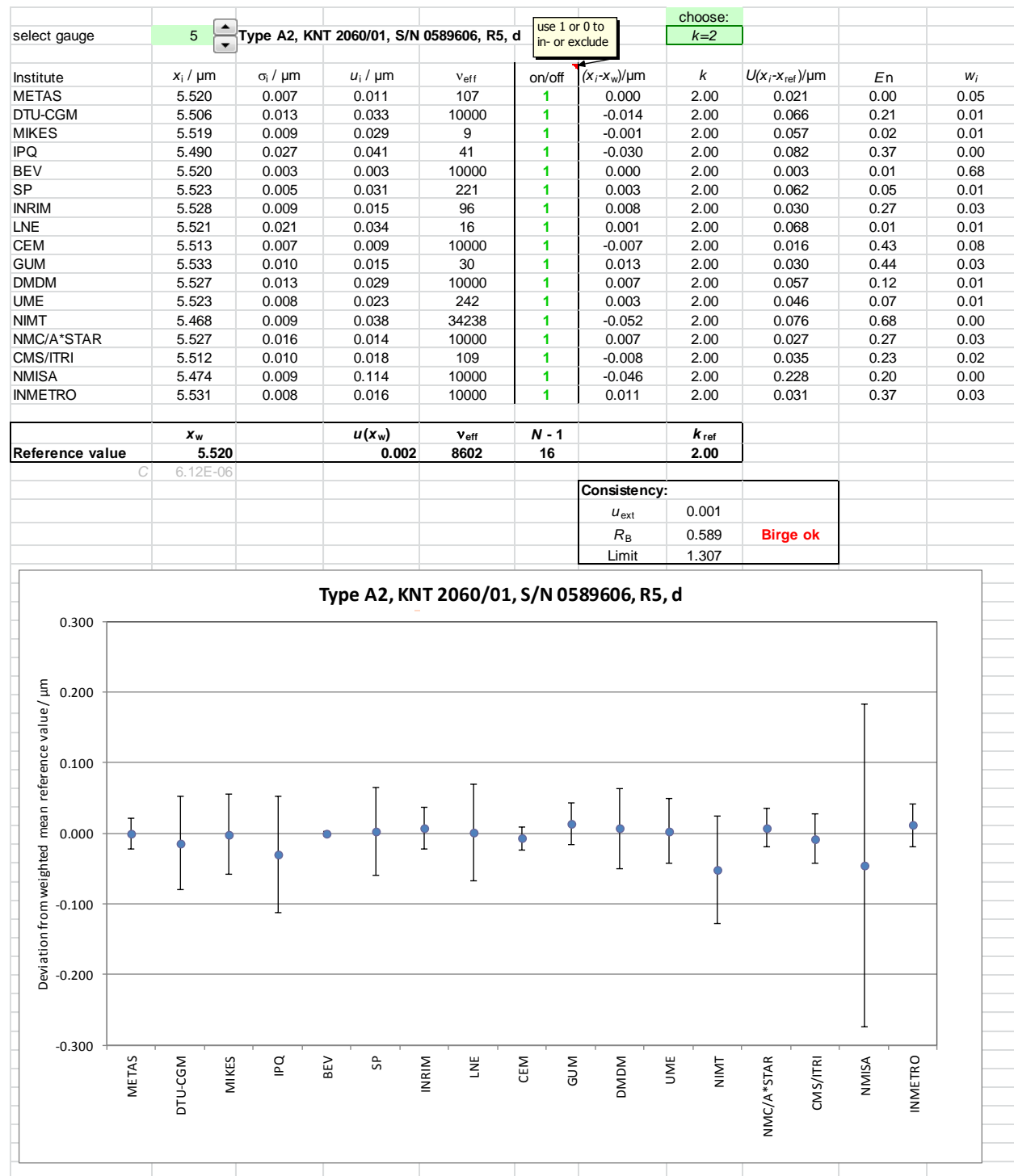
In the following, an extract of the Excel table *EURAMET.L-K8.2013-evaluation.xlsx* is given for each standard and each measurand. Laboratories starting with the largest  $E_n$  values were excluded (highlighted) until consistency according to the Birge ratio criterion was reached.  $E_n$  values larger than 1 are highlighted. Tables show final values of  $x_i$  and  $E_n$  for consistent Birge ratio  $R_B$ . All graphs show the deviations ( $x_i - x_w$ ) from the weighted mean key comparison reference value in  $\mu\text{m}$  with uncertainties expanded with  $k = 2$ .



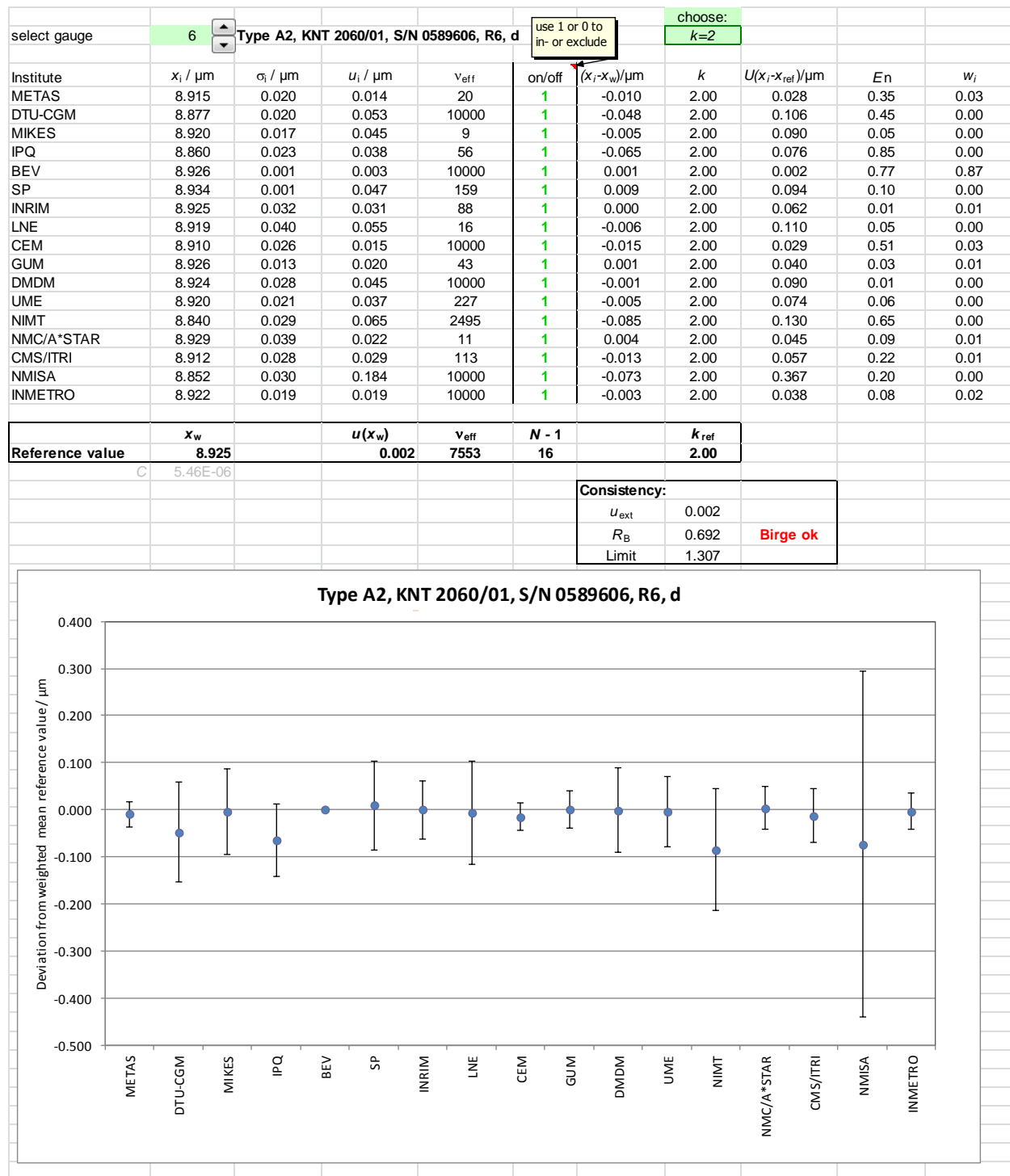


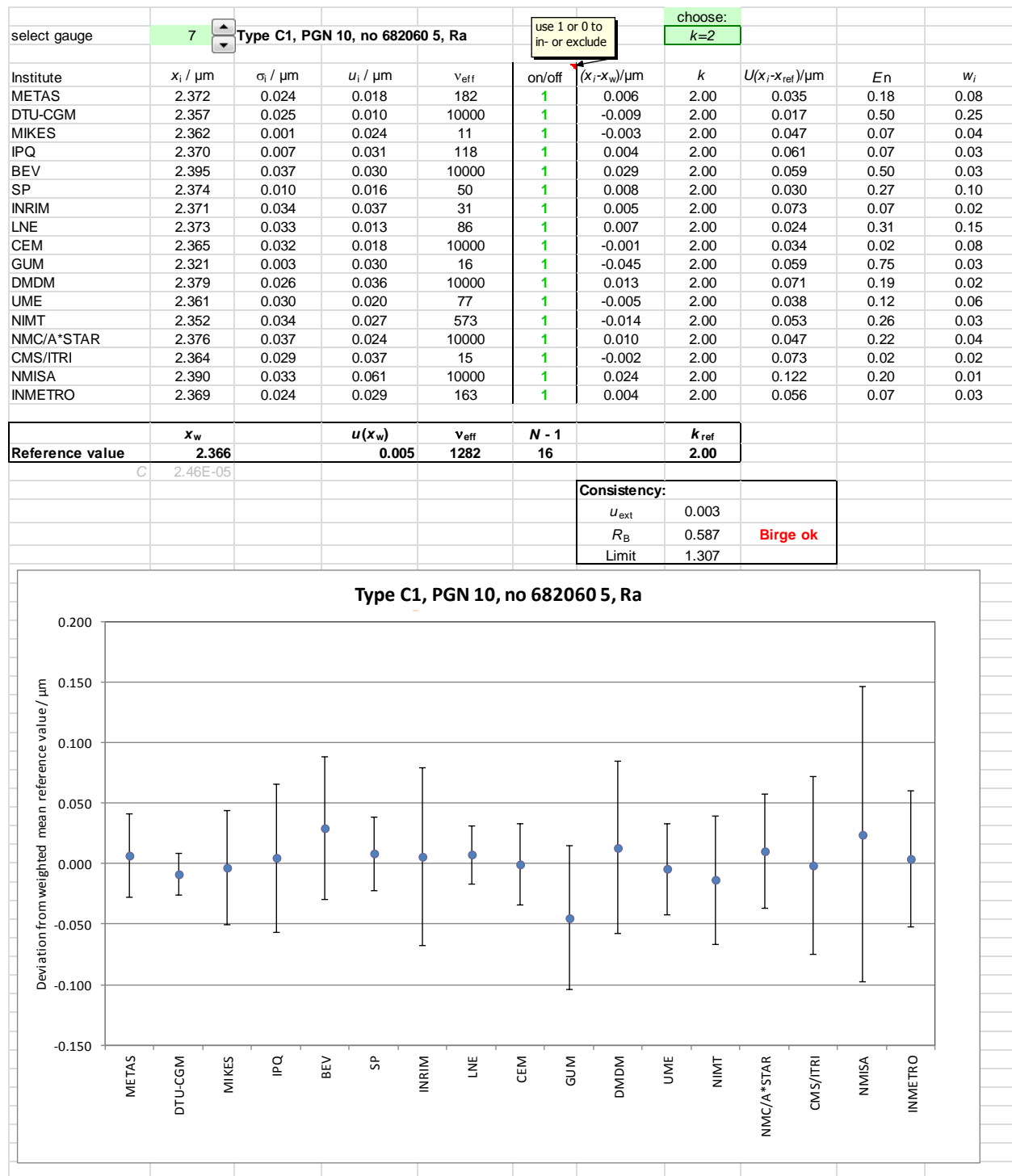


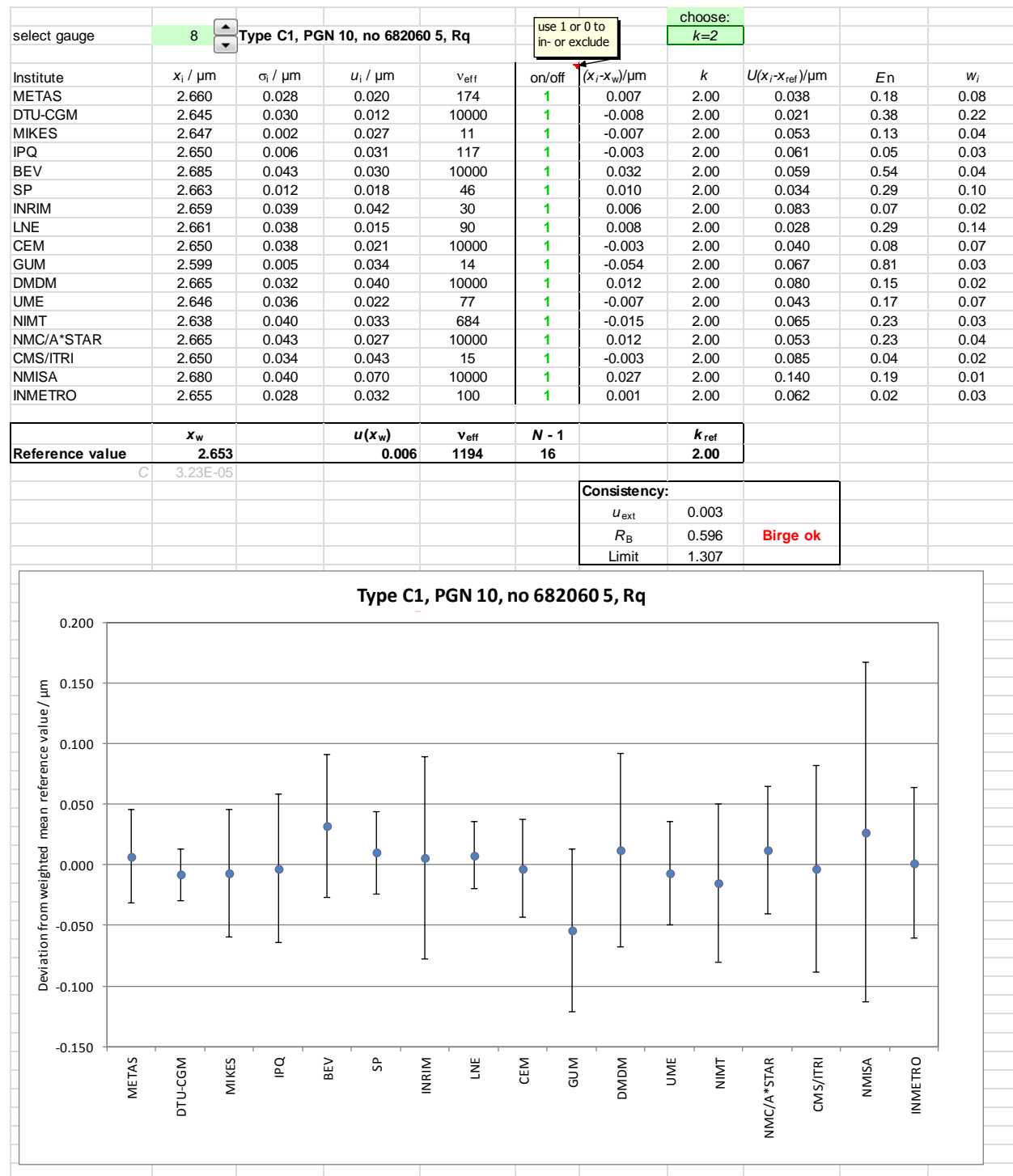


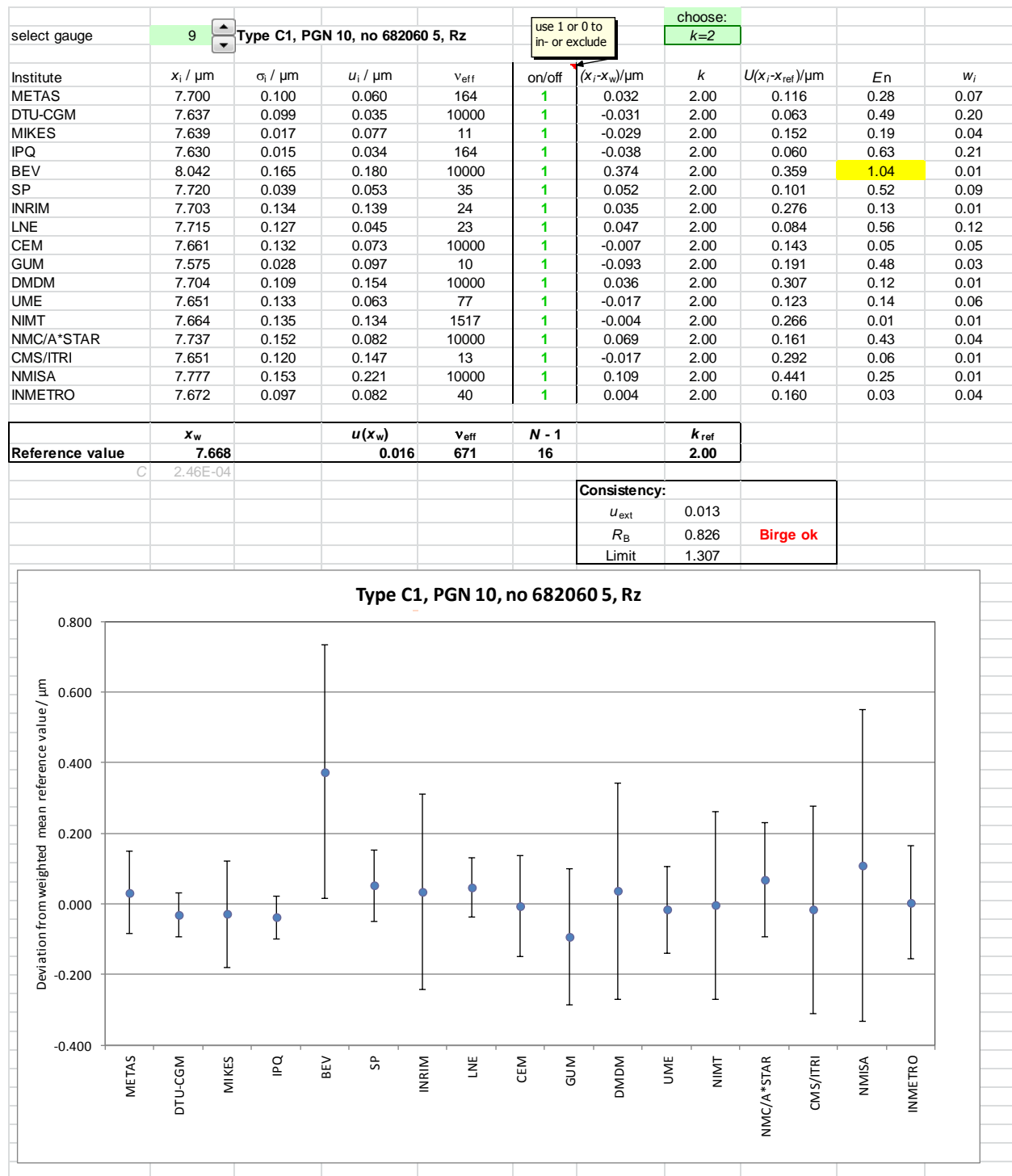


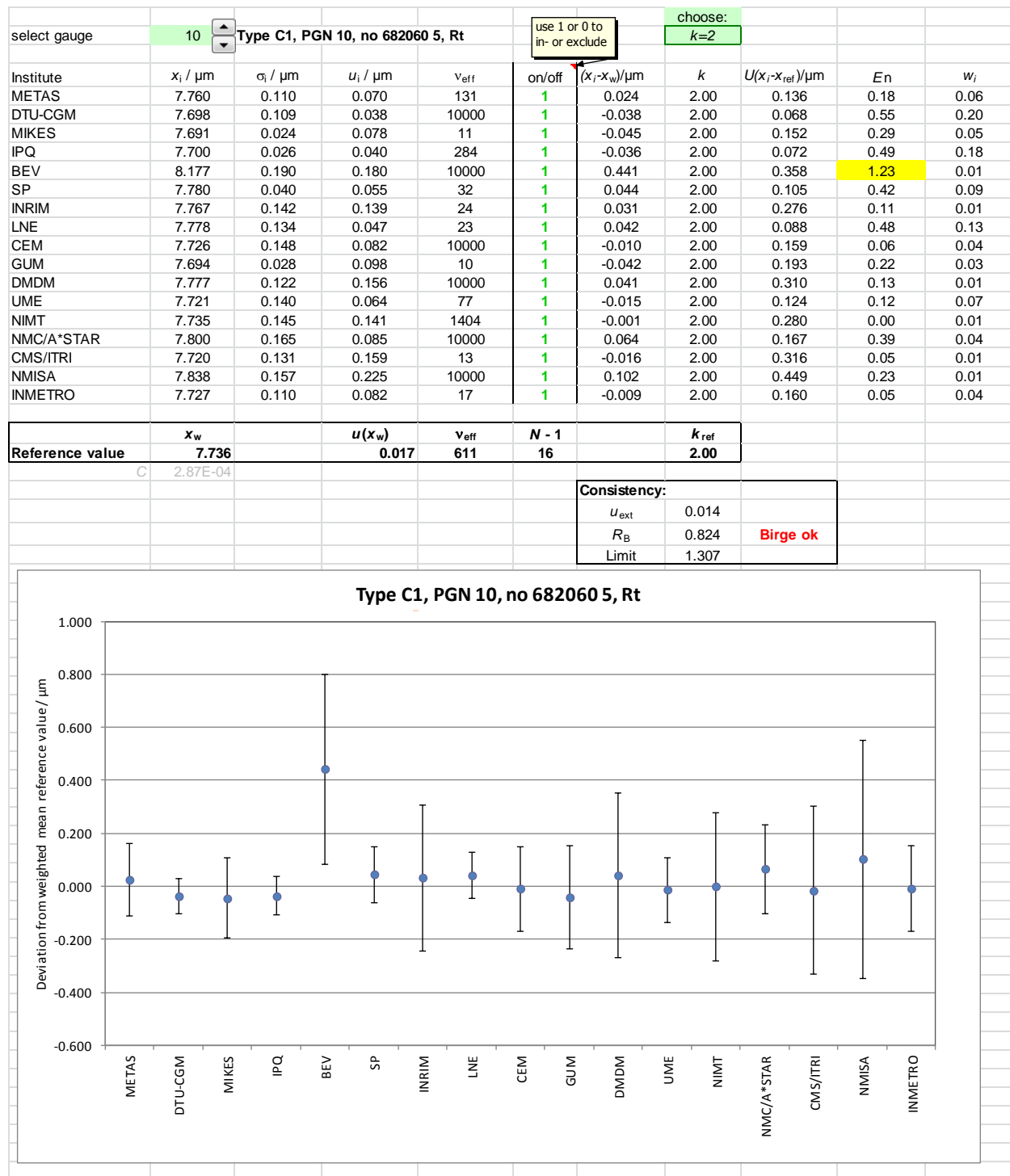


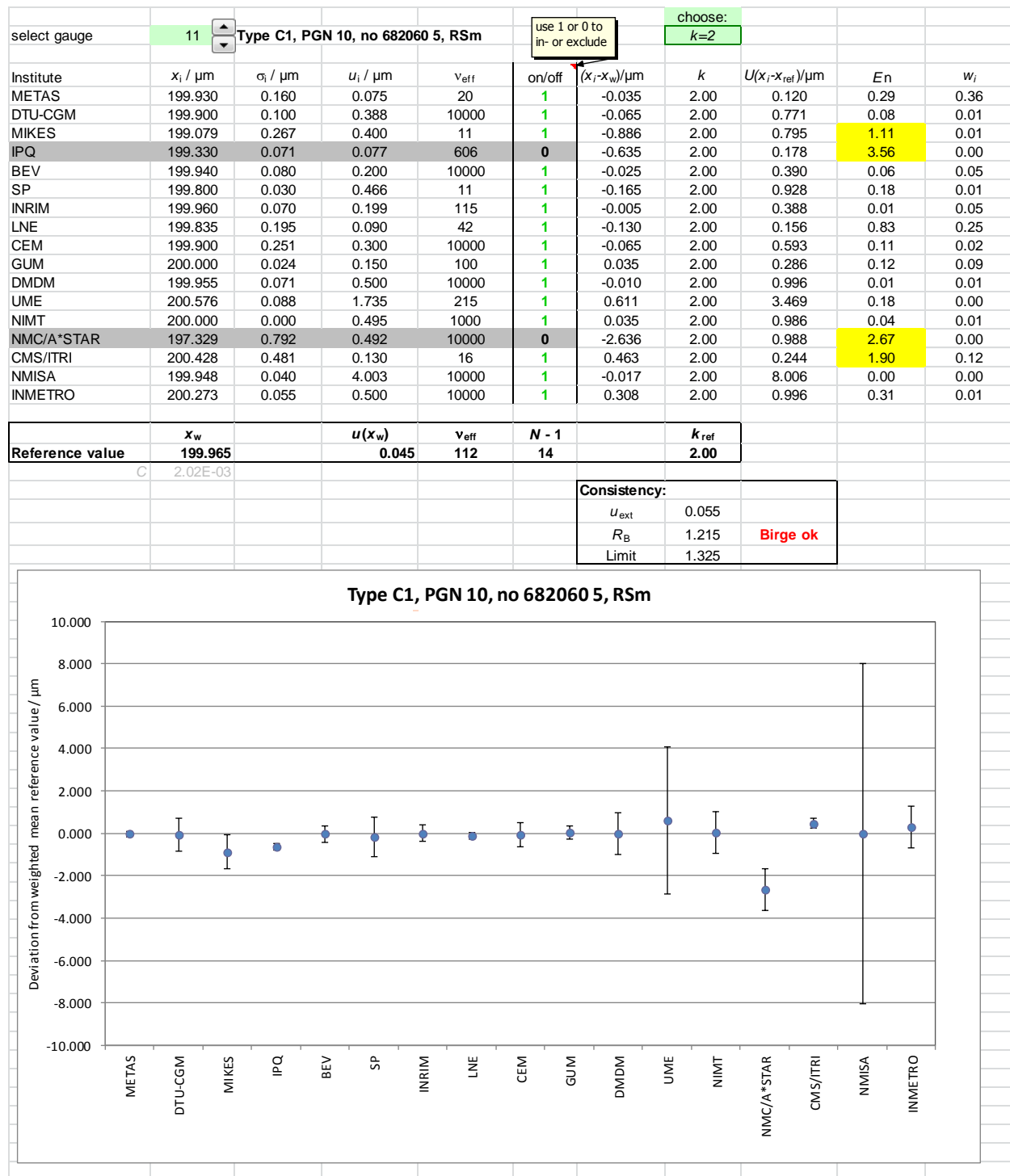


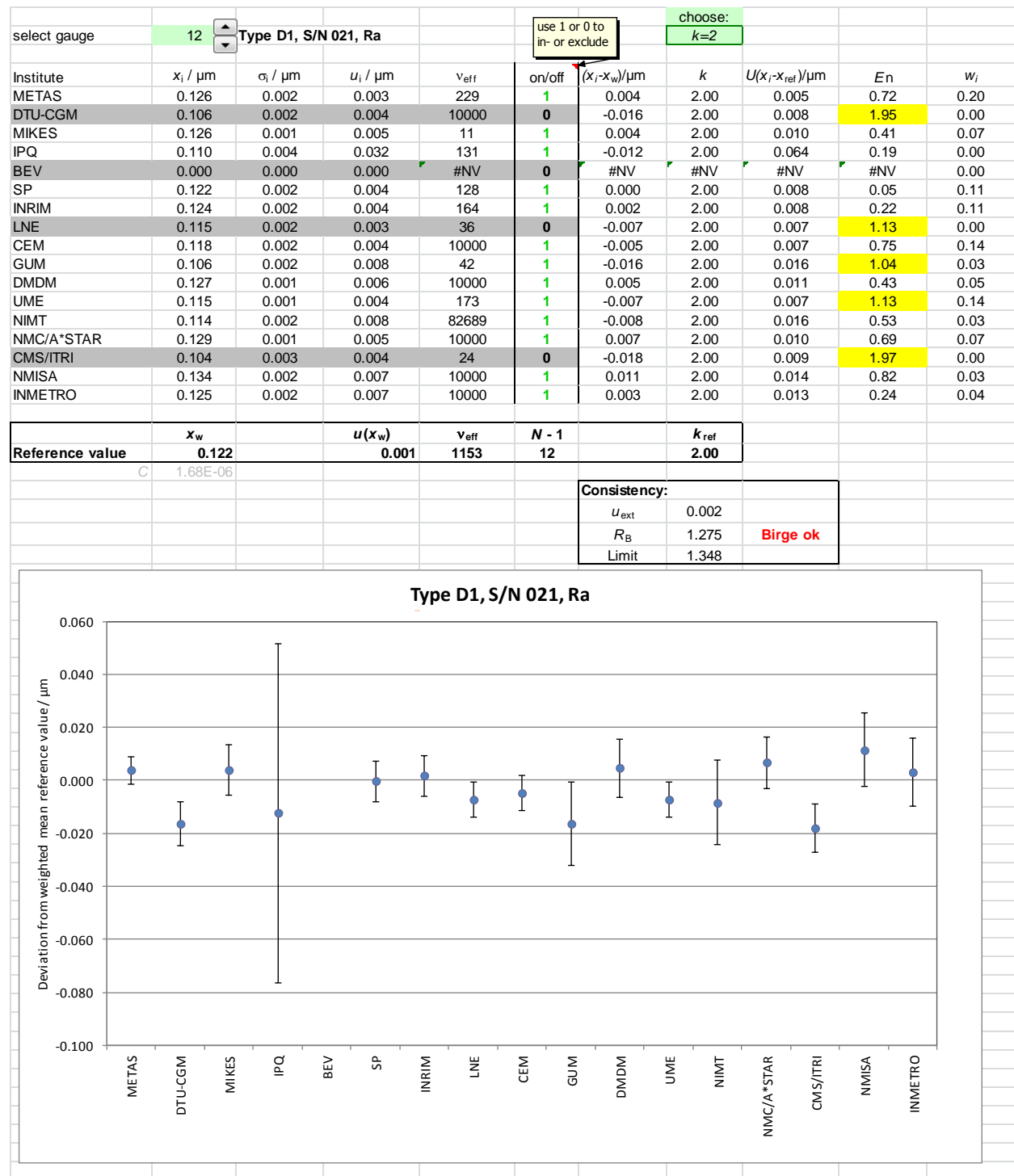


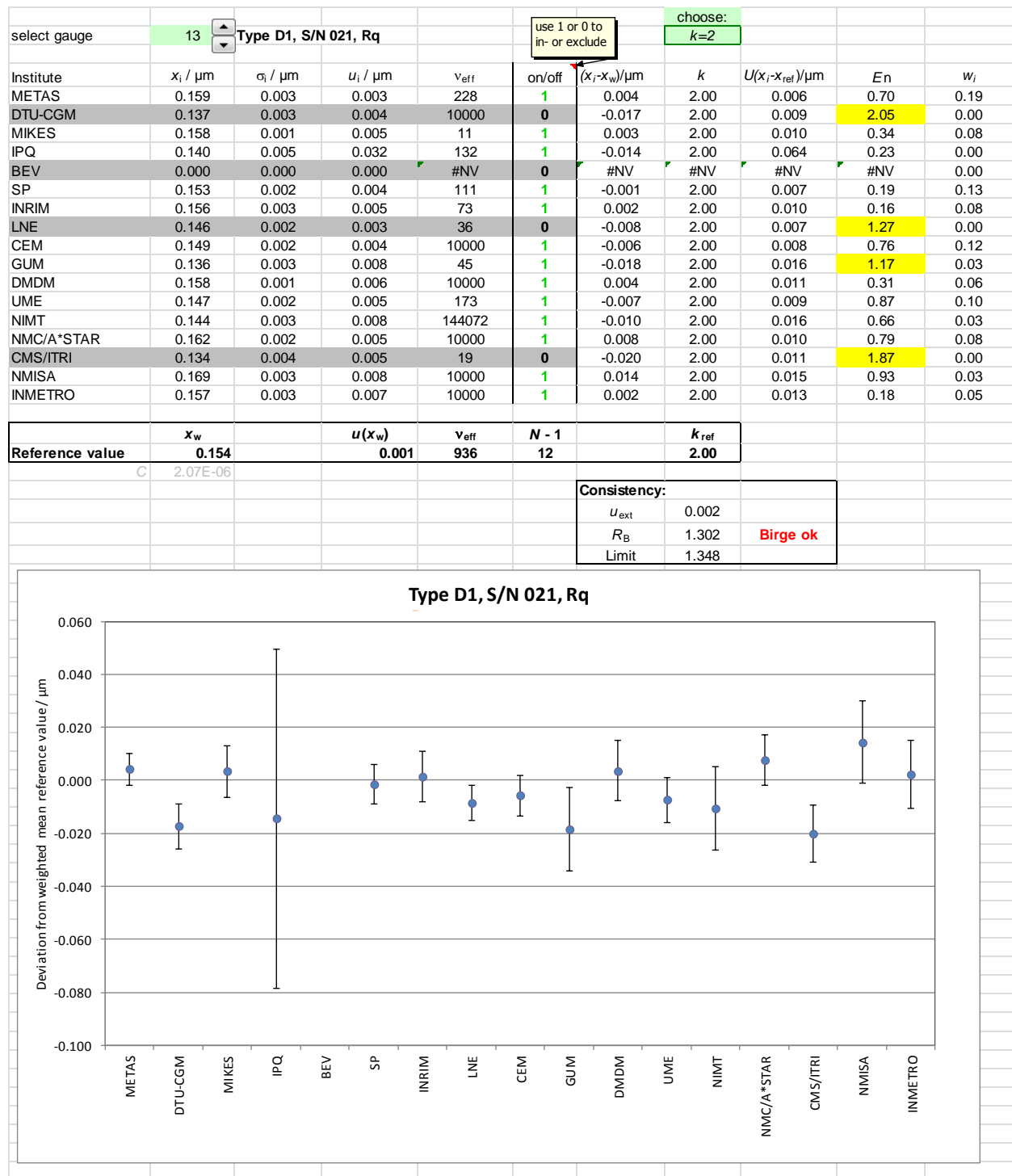




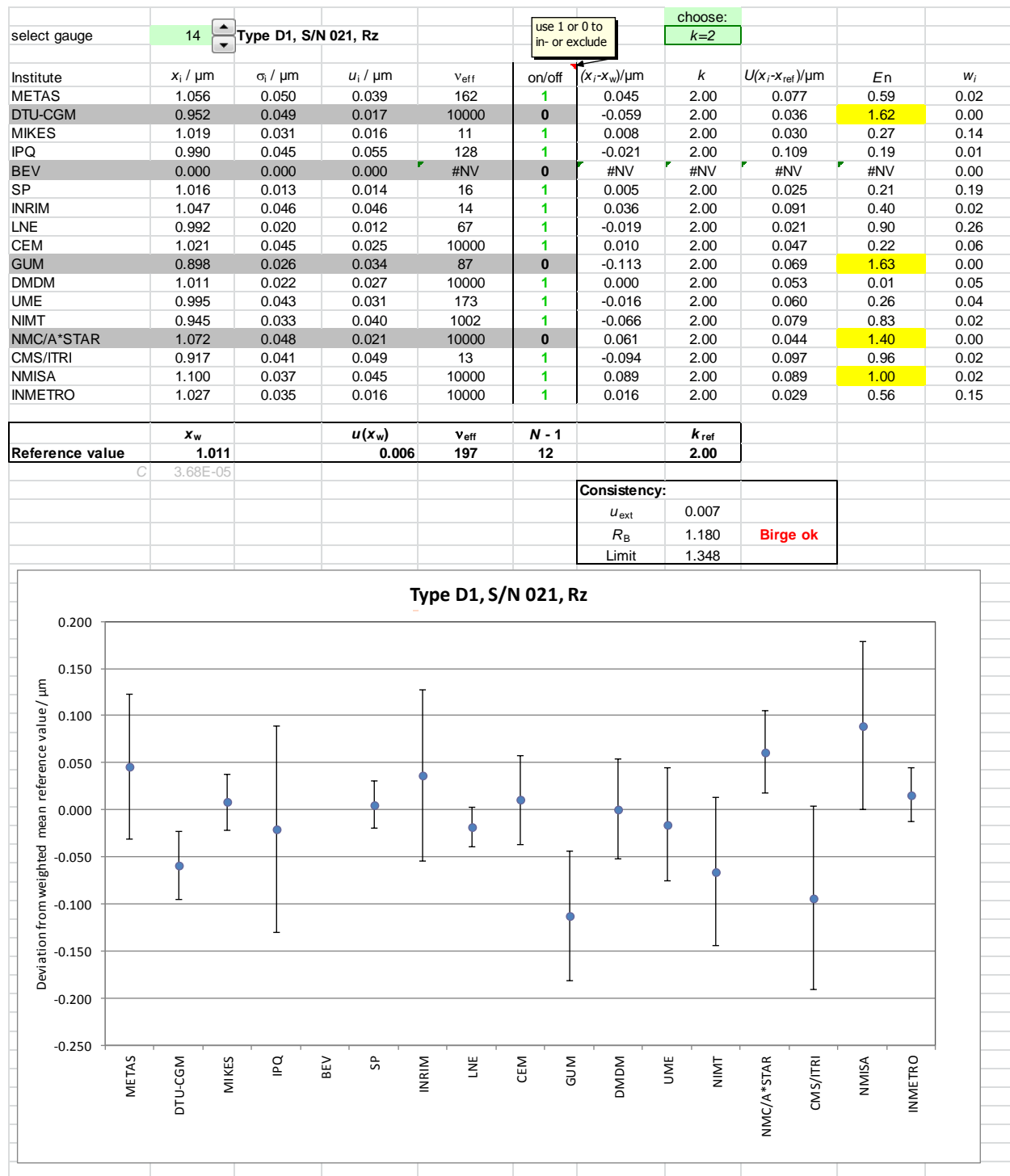


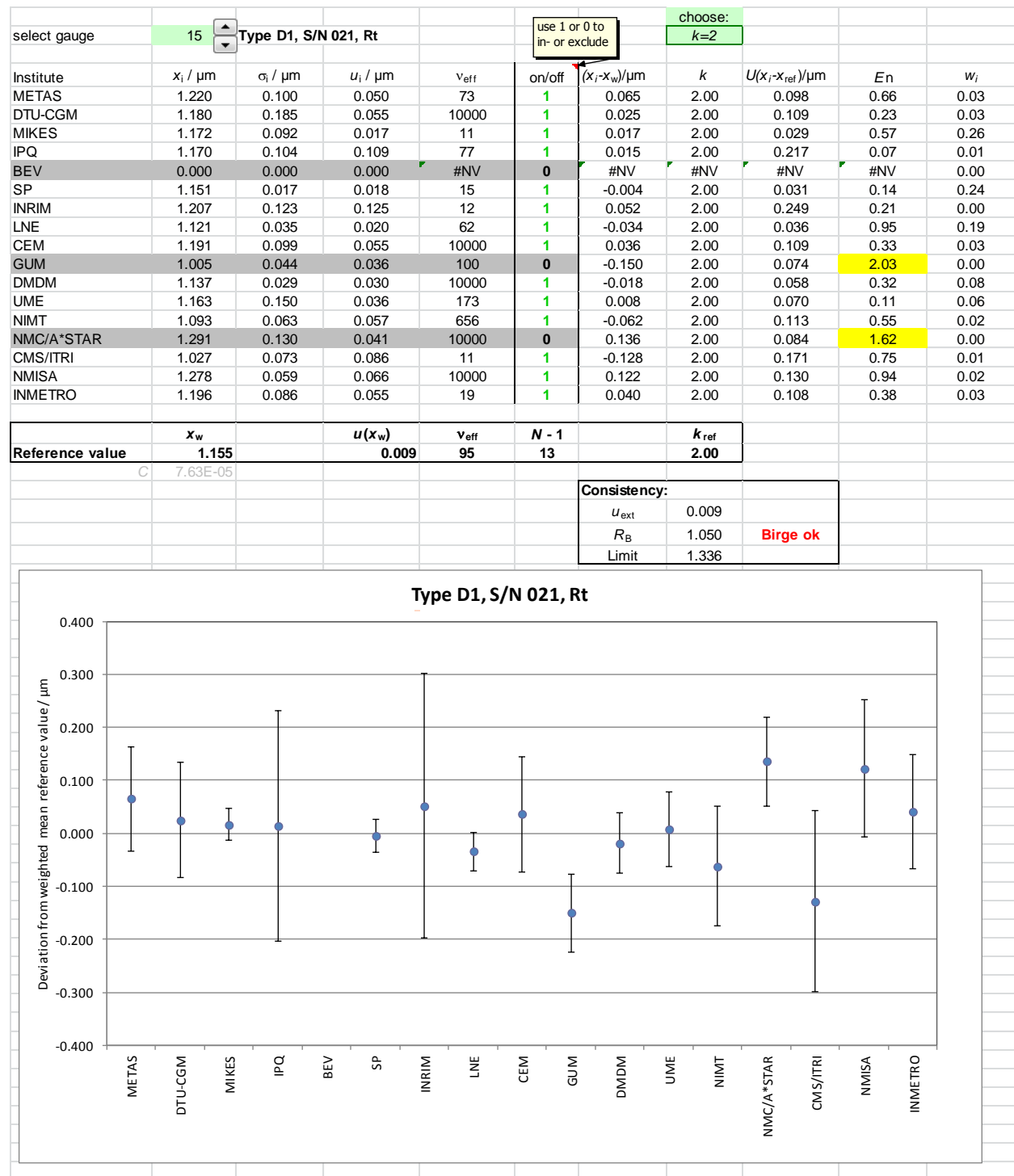


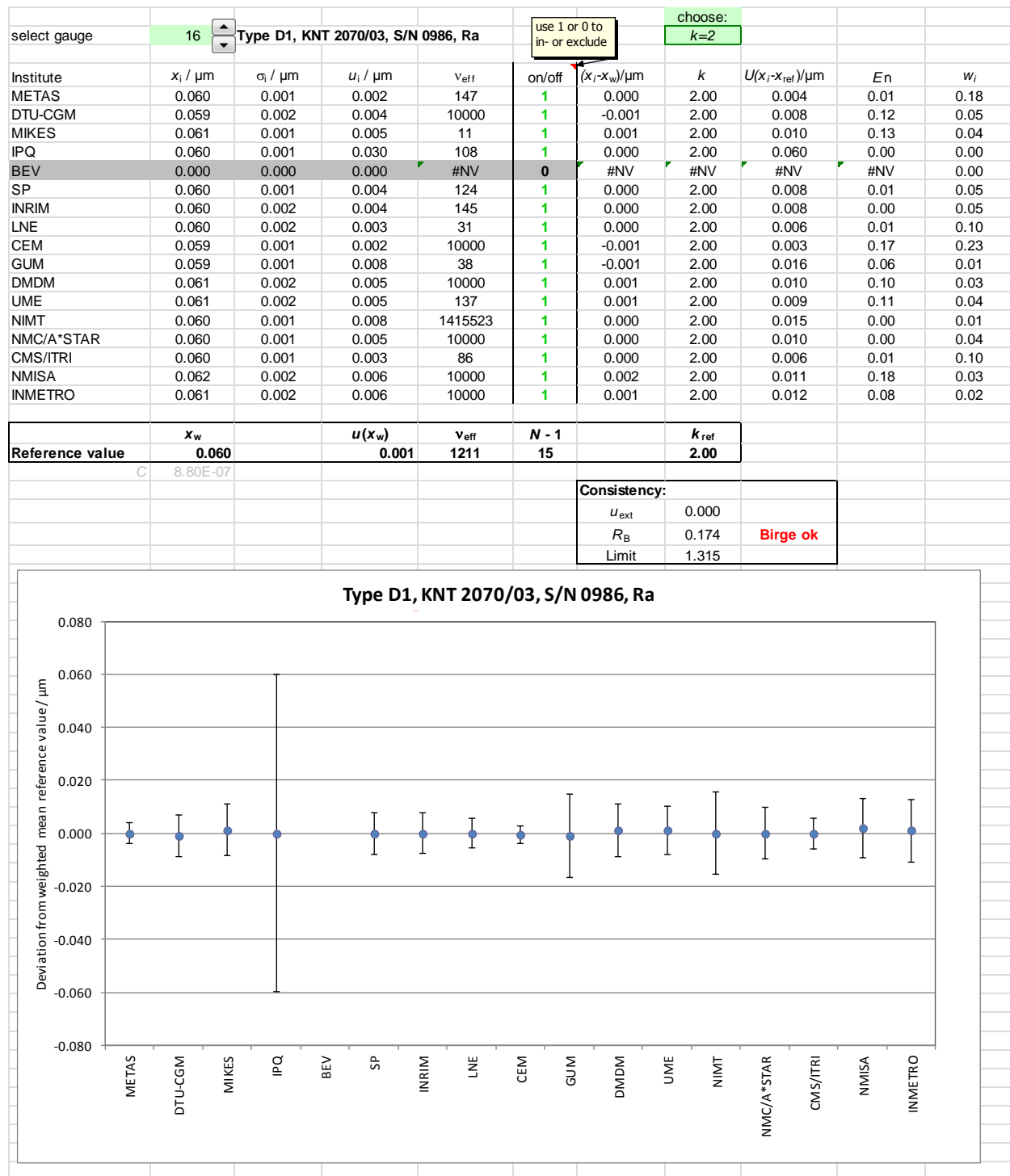


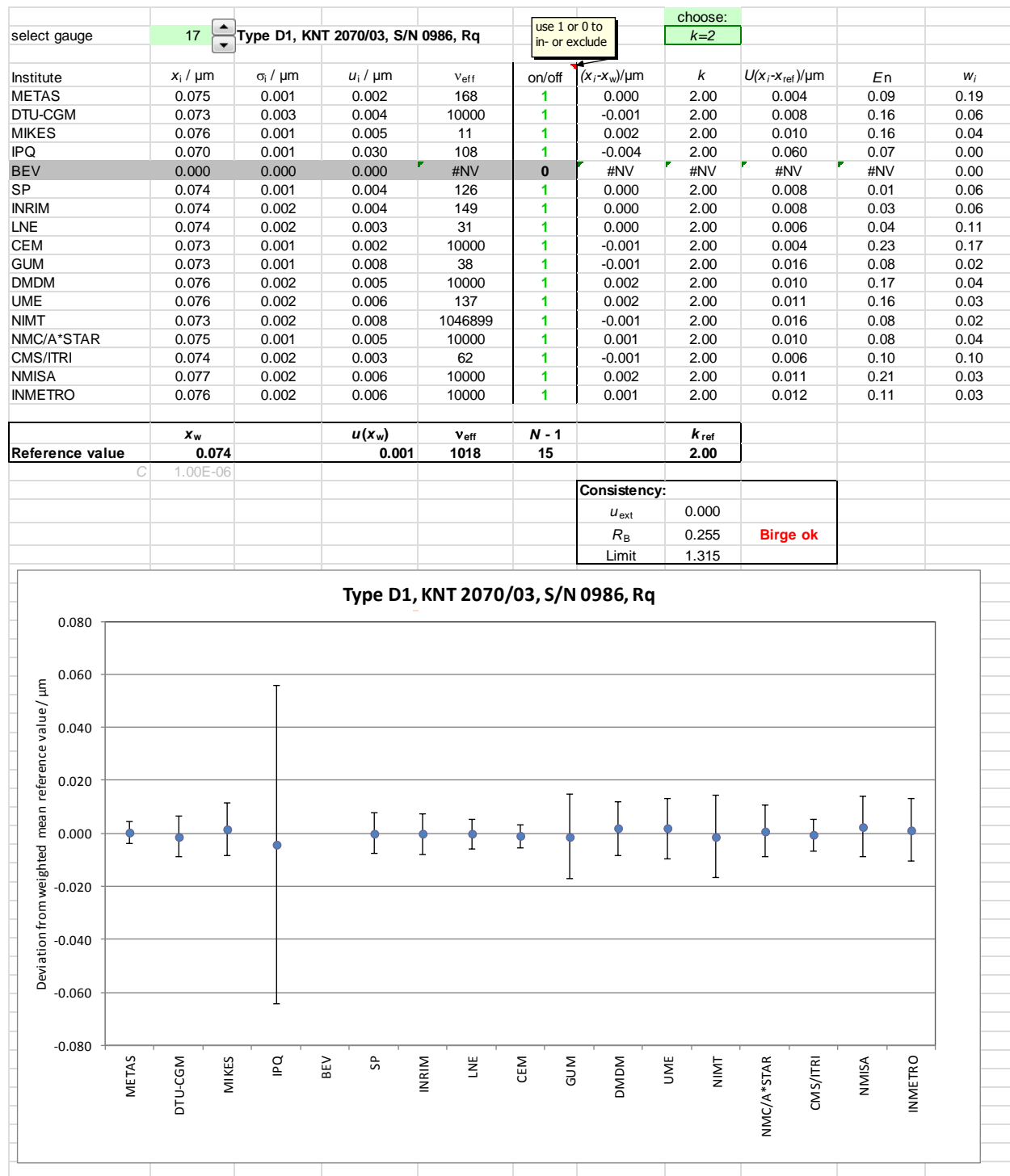


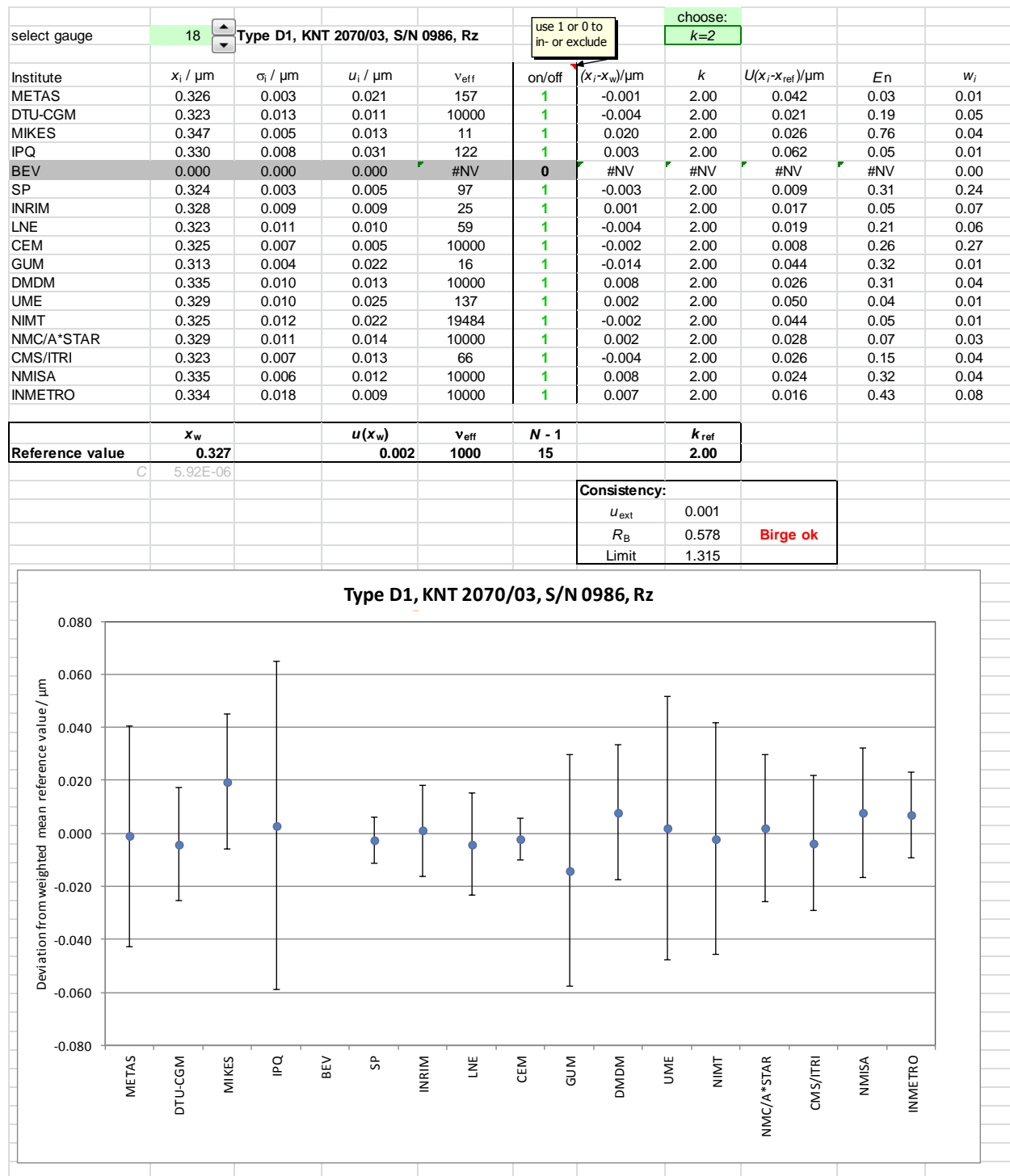


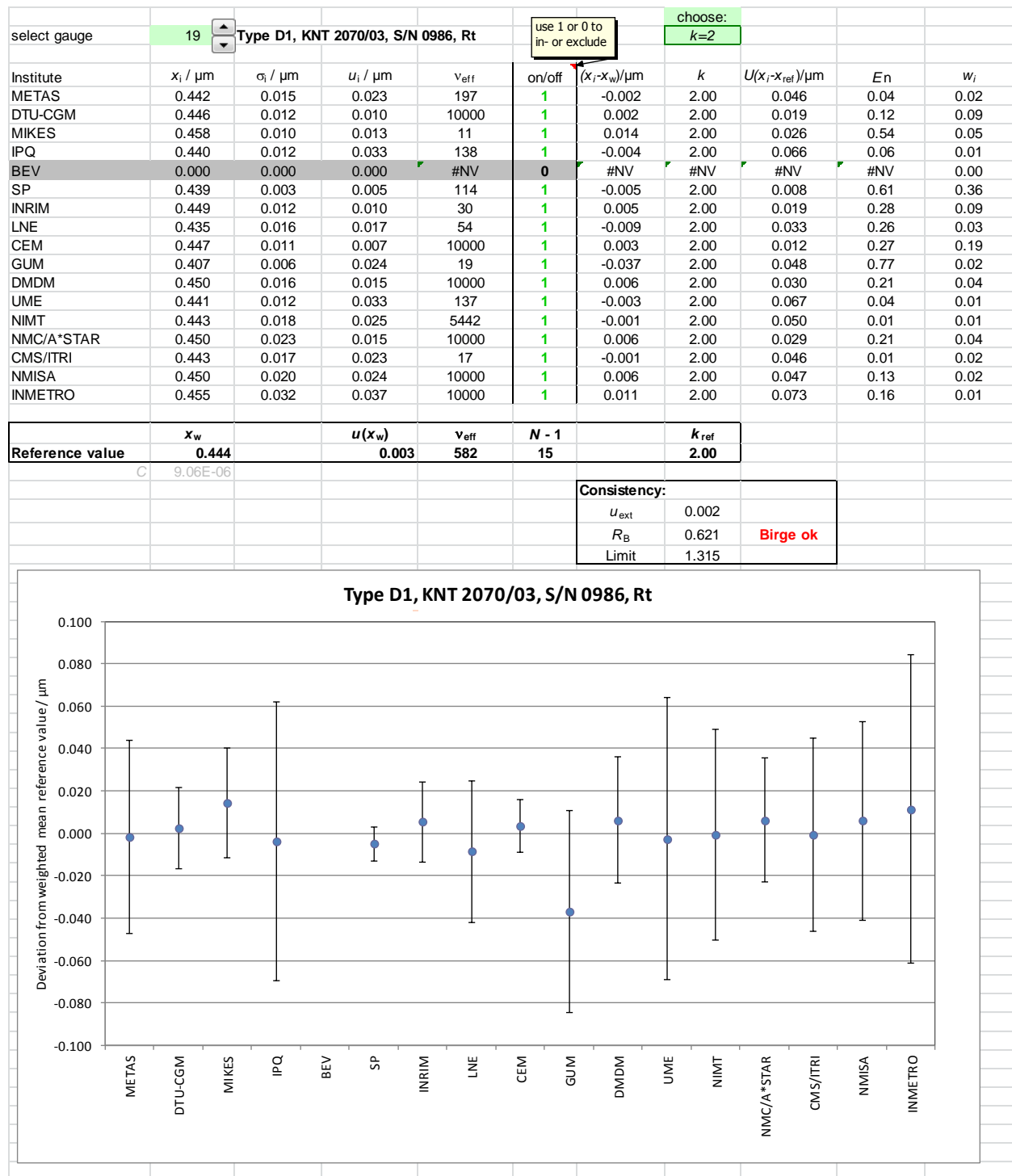


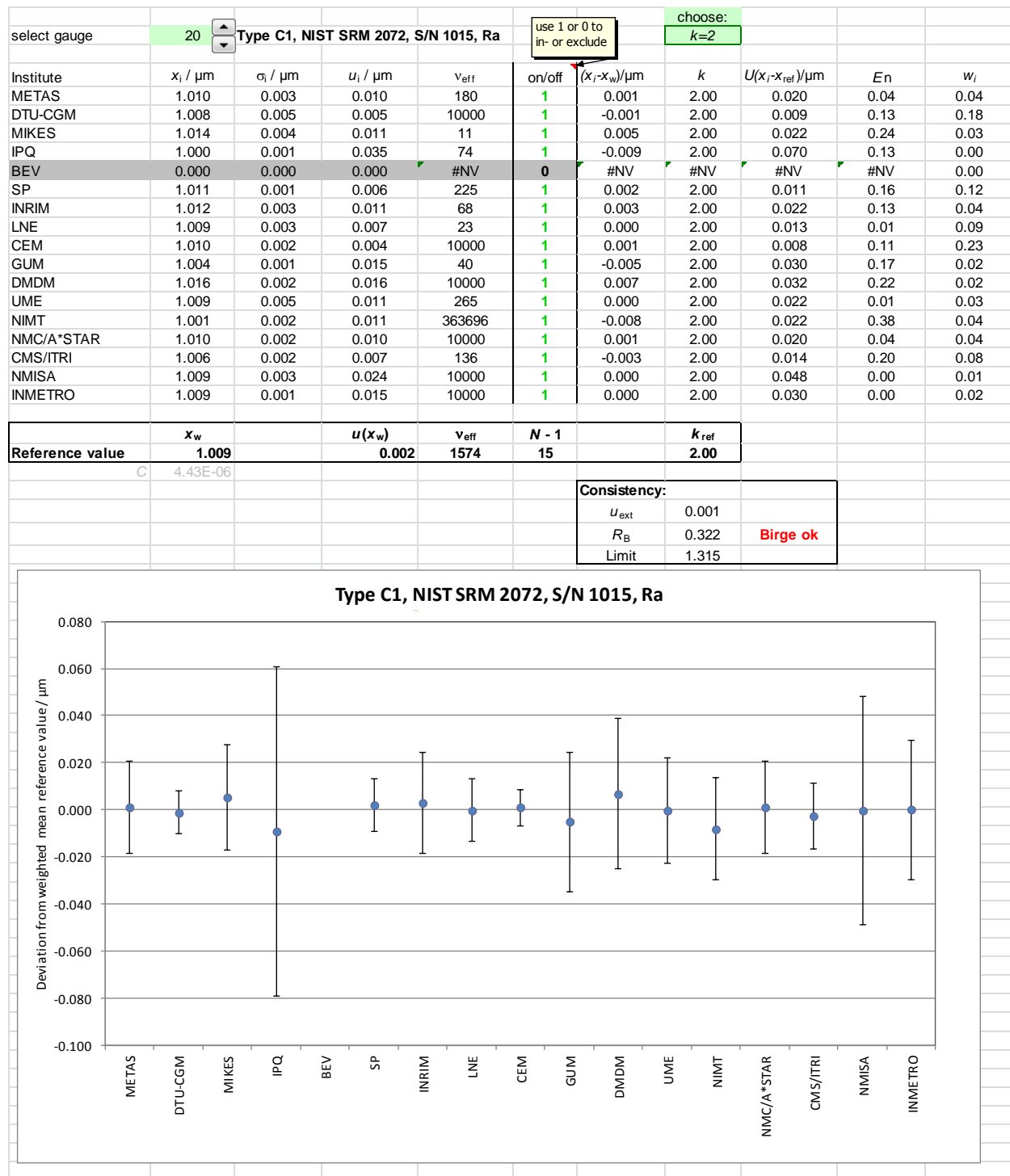


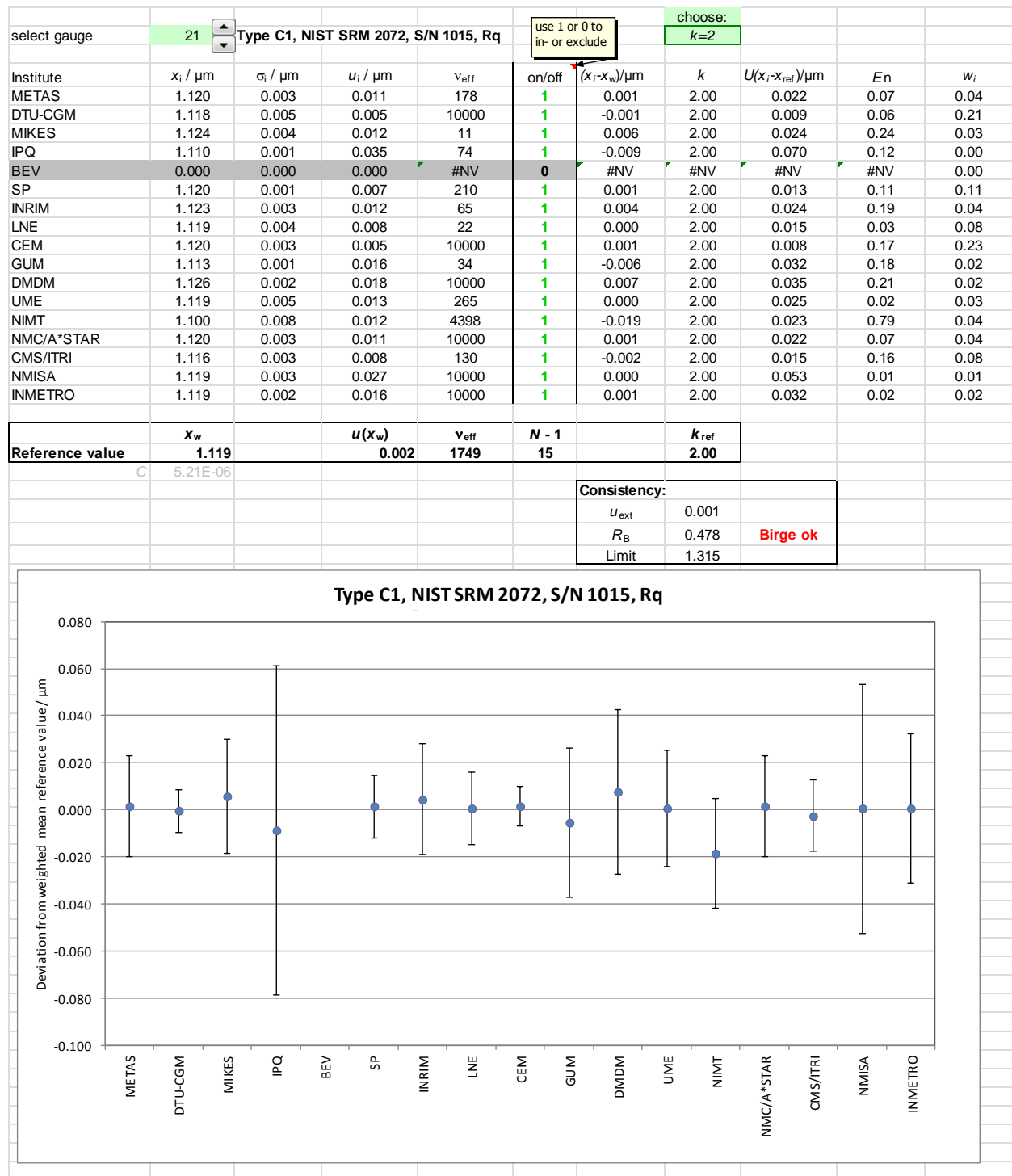




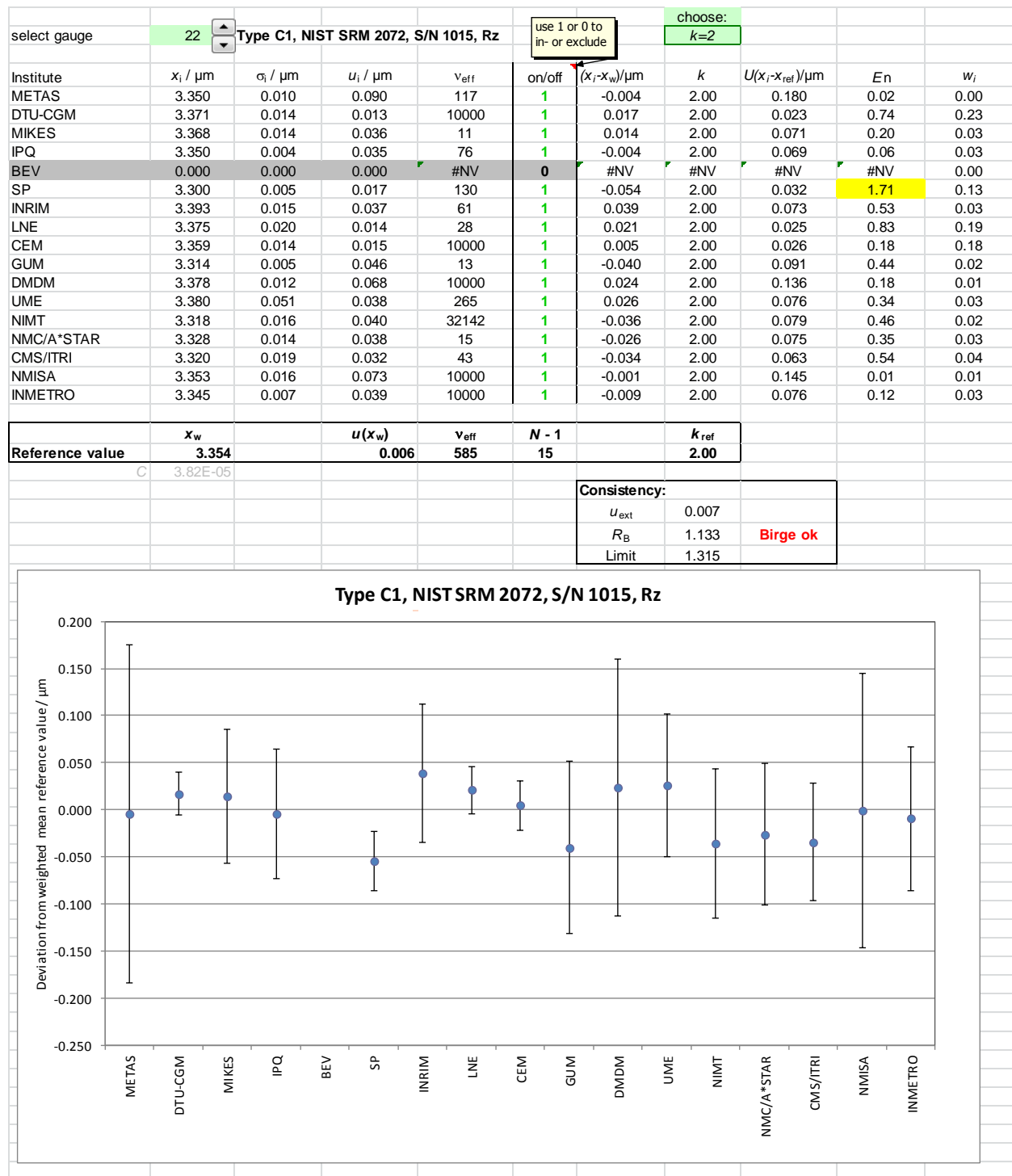


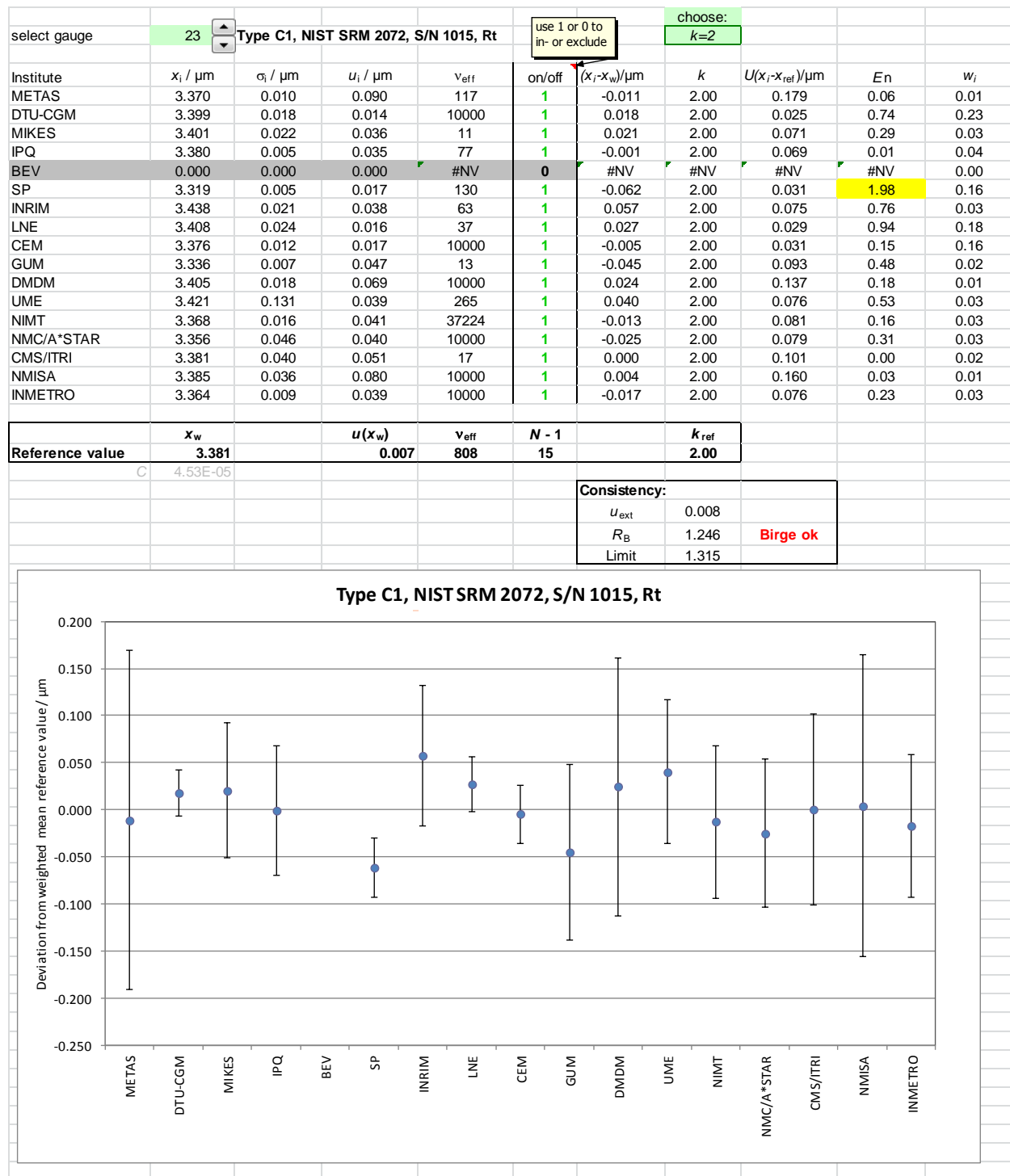


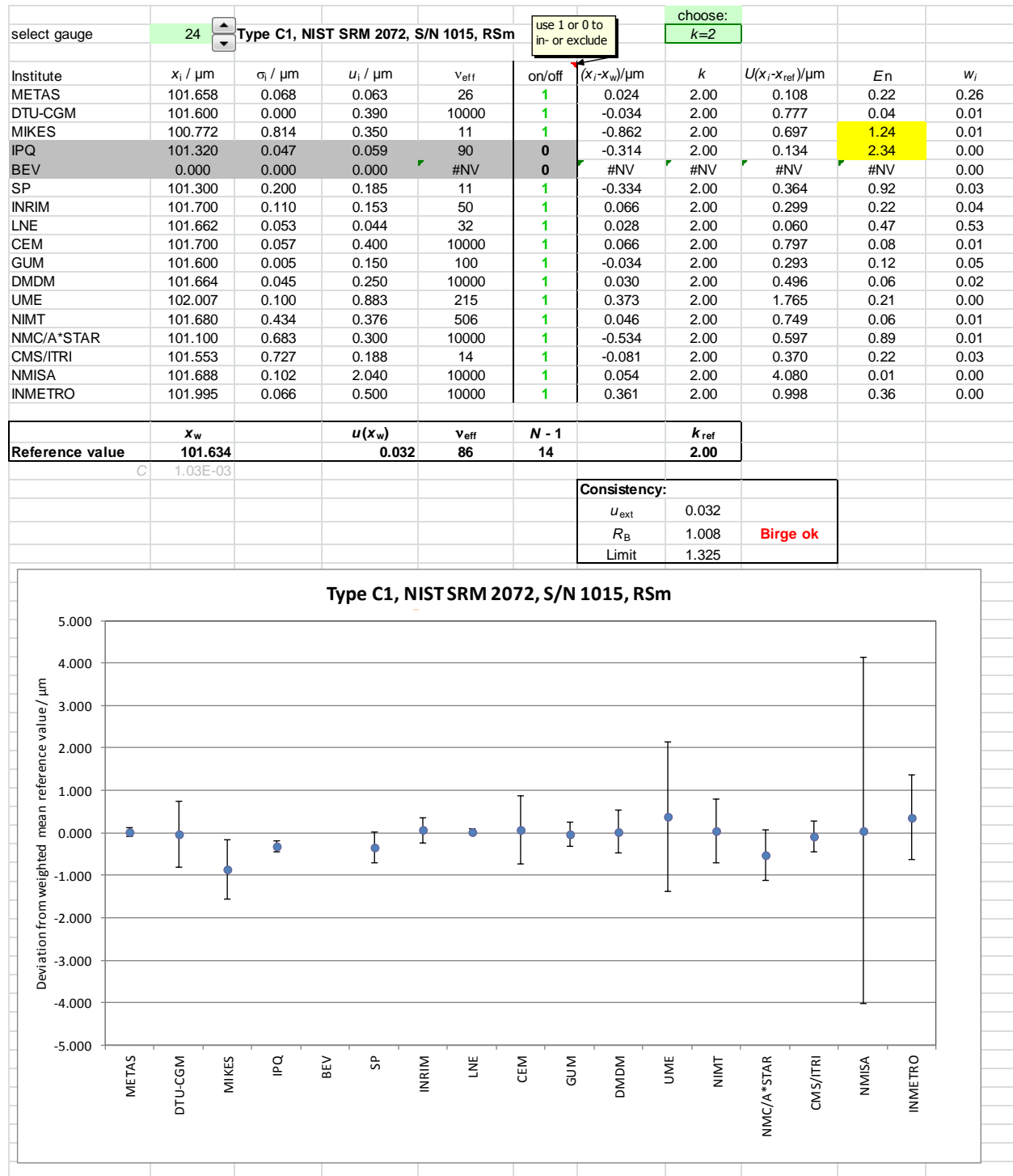












### 8.3 Summary of the $E_n$ values

In Table 5 the  $E_n$  values as shown in the tables of section 8.2 (i.e. after exclusion of inconsistent results) are summarized, with  $E_n > 1$  highlighted.

Table 5.  $E_n$  values of the originally reported results.

Institute	Type A2, KNT 2060/01, S/N 0589606						Type C1, PGN 10, no 682060 5				
	R1, d	R2, d	R3, d	R4, d	R5, d	R6, d	Ra	Rq	Rz	Rt	RSm
METAS	0.01	0.26	0.06	0.09	0.00	0.35	0.18	0.18	0.28	0.18	0.29
DTU-CGM	0.11	0.20	0.14	0.47	0.21	0.45	0.50	0.38	0.49	0.55	0.08
MIKES	0.22	0.16	0.29	0.00	0.02	0.05	0.07	0.13	0.19	0.29	1.11
IPQ	0.11	0.15	0.67	1.15	0.37	0.85	0.07	0.05	0.63	0.49	3.56
BEV	1.84	1.04	1.68	0.92	0.01	0.77	0.50	0.54	1.04	1.23	0.06
SP	0.41	0.12	0.16	0.03	0.05	0.10	0.27	0.29	0.52	0.42	0.18
INRIM	0.55	0.04	0.33	0.06	0.27	0.01	0.07	0.07	0.13	0.11	0.01
LNE	0.14	0.15	0.26	0.21	0.01	0.05	0.31	0.29	0.56	0.48	0.83
CEM	0.41	0.42	0.52	0.32	0.43	0.51	0.02	0.08	0.05	0.06	0.11
GUM	0.24	0.19	0.44	0.07	0.44	0.03	0.75	0.81	0.48	0.22	0.12
DMDM	0.50	0.39	0.17	0.05	0.12	0.01	0.19	0.15	0.12	0.13	0.01
UME	0.10	0.21	0.05	0.20	0.07	0.06	0.12	0.17	0.14	0.12	0.18
NIMT	0.30	0.20	0.69	0.69	0.68	0.65	0.26	0.23	0.01	0.00	0.04
NMC/A*STAR	0.05	0.11	0.07	0.06	0.27	0.09	0.22	0.23	0.43	0.39	2.67
CMS/ITRI	0.61	0.55	0.71	0.53	0.23	0.22	0.02	0.04	0.06	0.05	1.90
NMISA	2.19	1.13	1.07	0.55	0.20	0.20	0.20	0.19	0.25	0.23	0.00
INMETRO	0.18	0.02	0.10	0.24	0.37	0.08	0.07	0.02	0.03	0.05	0.31

Institute	Type D1, S/N 021				Type D1, KNT 2070/03, S/N 0986				Type C1, NIST SRM 2072, S/N 1015				
	Ra	Rq	Rz	Rt	Ra	Rq	Rz	Rt	Ra	Rq	Rz	Rt	RSm
METAS	0.72	0.70	0.59	0.66	0.01	0.09	0.03	0.04	0.04	0.07	0.02	0.06	0.22
DTU-CGM	1.95	2.05	1.62	0.23	0.12	0.16	0.19	0.12	0.13	0.06	0.74	0.74	0.04
MIKES	0.41	0.34	0.27	0.57	0.13	0.16	0.76	0.54	0.24	0.24	0.20	0.29	1.24
IPQ	0.19	0.23	0.19	0.07	0.00	0.07	0.05	0.06	0.13	0.12	0.06	0.01	2.34
BEV													
SP	0.05	0.19	0.21	0.14	0.01	0.01	0.31	0.61	0.16	0.11	1.71	1.98	0.92
INRIM	0.22	0.16	0.40	0.21	0.00	0.03	0.05	0.28	0.13	0.19	0.53	0.76	0.22
LNE	1.13	1.27	0.90	0.95	0.01	0.04	0.21	0.26	0.01	0.03	0.83	0.94	0.47
CEM	0.75	0.76	0.22	0.33	0.17	0.23	0.26	0.27	0.11	0.17	0.18	0.15	0.08
GUM	1.04	1.17	1.63	2.03	0.06	0.08	0.32	0.77	0.17	0.18	0.44	0.48	0.12
DMDM	0.43	0.31	0.01	0.32	0.10	0.17	0.31	0.21	0.22	0.21	0.18	0.18	0.06
UME	1.13	0.87	0.26	0.11	0.11	0.16	0.04	0.04	0.01	0.02	0.34	0.53	0.21
NIMT	0.53	0.66	0.83	0.55	0.00	0.08	0.05	0.01	0.38	0.79	0.46	0.16	0.06
NMC/A*STAR	0.69	0.79	1.40	1.62	0.00	0.08	0.07	0.21	0.04	0.07	0.35	0.31	0.89
CMS/ITRI	1.97	1.87	0.96	0.75	0.01	0.10	0.15	0.01	0.20	0.16	0.54	0.00	0.22
NMISA	0.82	0.93	1.00	0.94	0.18	0.21	0.32	0.13	0.00	0.01	0.01	0.03	0.01
INMETRO	0.24	0.18	0.56	0.38	0.08	0.11	0.43	0.16	0.00	0.02	0.12	0.23	0.36

### 8.4 Discussion of results

In spite of a relatively large number of inconsistent results, the overall agreement is considered to be satisfactory. A number of inconsistent results can be explained (see section 8.5).

- 32 out of 395 results are not consistent with the reference value, i.e.  $E_n > 1$ .
- 11 out of 17 laboratories had at least one inconsistent result.
- The largest number (15) of inconsistent results was found on the standard with the least quality, i.e. Rubert D1.

- The degradation of the quality of the standards in the course of the comparison due to surface damages did hardly affect the measurement results. There is no clear trend visible from the first to the last participant, even the last participant achieved excellent results, and the stability measurements made by the pilot were all consistent (see section 6.1).
- Pt values for the type A2 standard were part of the protocol in order to be compatible to the protocol of the preceding comparison EURAMET.L-K8, but do not correspond to the standardized profile depth. They were included in the evaluation spreadsheet of this comparison, but are not part of the draft B report. Therefore no further analysis is carried out on this parameter.

## 8.5 Changes to results after Draft A report

After sending draft A report, the pilot received three requests to change values or uncertainties:

### 8.5.1 BEV request from 13.02.2015

*I noticed to actually have sent values for the wrong measurand for the type A2 standard. Originally our values are for the central trace (as written on our report) where "the average result together with the standard deviation" was requested. This makes only minor changes to the actual values but the standard deviation is of course much higher (and also the uncertainty).*

*I have re-evaluated the d parameter according to this.*

Attached was a report file with slightly different values and increased uncertainties.

### 8.5.2 NMISA comment from 06.03.2015 and report from 22.04.2015

*I checked the data as the groove stds was far out and did not expect it. The laboratory had a Taylor Hobson Form Talysurf series which was upgraded to a PGI system with a newer version of the same software only months before the inter-comparison. While performing the measurements for the groove standard, Type A2, KNT 2060/01, S/N 0589606, a mistake was made in the analysis of the results. The filter is selected in two places, firstly, the primary filter and in the next instance, instead of no filter in place, we selected the primary filter again.*

*Our results were thus systematically lower than should be. This came to light when Draft A of the inter-comparison report was published. A re-analysis of all the measurements for the groove depth standard was done and the results are attached.*

Attached was a report file with values changed accordingly.

### 8.5.3 IPQ request from 12.03.2015

*I ask if it is possible to consider the following updates: I detect a mistake in the IPQ reported values for the surface roughness standard Type A2, KNT 2060/01, S/N 0589606, R4, d (instead of 2.64  $\mu\text{m}$  it is 2.68  $\mu\text{m}$ ). I also made an update of the measurement uncertainty for the parameter RSm of the two standards (Type C1, PGN 10, no 682060 5, RSm and Type C1, NIST SRM 2072, S/N 1015, RSm) adding a new uncertainty component.*

Additional information was received from IPQ to justify and support the above mentioned changes. The uncertainties of IPQ for RSm were changed from 77 nm to 321 nm and from 59 nm to 214 nm, respectively, introduced in the spreadsheet *EURAMET.L-K8.2013-revised values.xlsx* and for the analysis in section 8.6.3.

## 8.6 Comments received after Draft B.1 report

After sending draft B.1 report, the pilot received the following comments:

### 8.6.1 INMETRO comment from 29.04.2015

*I am really sorry, but I made a rough mistake when declaring our measurement uncertainties. Instead of sending you the "uc" uncertainties, I declared the expanded ones (U). All our expanded uncertainties are based in the ones that we have in the KCDB App. C.*

*For the calibration of depth setting standards they are:  
(20+2H) nm; H=d or Pt (in  $\mu\text{m}$ )*

*For the calibration of roughness standards they are:  
(10+20P) nm; P=vertical parameters (in  $\mu\text{m}$ )*

*If it would be possible, I ask you, please, to correct our "ui" values in the tables, dividing them by 2, as well plotting the graphs considering it.*

This is an obvious mistake. In order to get a more reliable evaluation of the reference values and the degrees of equivalence, the uncertainties of INMETRO were divided by 2, and all data presented in section 8.2 were updated.

### 8.6.2 NMC/A\*STAR comment from 18.05.2015

- 1) The supplier in Singapore upgraded the software and we at NMC completed the re-analysis of those raw data captured during the comparison measurement at NMC. It was confirmed that only RSm values were wrongly calculated. ...*
- 2) The RSm values of two comparison samples (PNG 10 and NIST SRM2072) were re-calculated and corresponding uncertainties were also slightly changed due to the change of the standard deviation. The results in detail are summarized in attachment, in which new RSm values of two samples are listed. ...*
- 3) Since our results (Rz & Rt) for the sample (Type D1, S/N 021) have the En value larger than 1, we need to study the root cause. As requested before, could you please kindly arrange to send the sample for us to do re-measurement at NMC?*

Attached were detailed reports on re-analysis of RSm-values. The following revised values were introduced in the spreadsheet *EURAMET.L-K8.2013-revised values.xlsx* and for the analysis in section 8.7:

Standard	Parameter	Value ( $\mu\text{m}$ )	$\sigma$ ( $\mu\text{m}$ )	uc (nm)	veff
PGN 10, no 682060 5,	RSm	199.978	0.058	442	$\infty$
NIST SRM 2072, S/N 1015	RSm	101.663	0.077	228	$\infty$

### 8.6.3 GUM comment from 19.05.2015

*We have once more checked very carefully our results, especially those concerning roughness standard type D1, SN 021. As you know this standard is of the worst quality with scratches and other damages. We have already noted the state of this standard in our first report.*

*While checking our printed measurements protocol we have noticed a mistake. Instead of giving you the real values of measurement uncertainties we claimed values given in our CMCs. Our measurements protocol prints both values for each roughness parameter. Usually these values are almost the same but at this case they have differed significantly. So if it is possible we would like to ask you to change our uncertainties values concerning Rz and Rt parameters of roughness standard type D1, SN 021. For Rz*

parameter we would like to change uncertainty value from 34 nm on 79 nm and for Rt parameter from 36 nm on 114 nm.

We want also to add that the standard deviation values for Rt and Rz parameters we have measured for this standard exceed the tolerance 3 % value given in the ISO 5436, 5,4 % (0,054  $\mu\text{m}$ ) for Rt parameter and 3,5 % (0,035  $\mu\text{m}$ ) for Rz parameter.

The above revised uncertainties were introduced in the spreadsheet *EURAMET.L-K8.2013-revised values.xlsx* and for the analysis in section 8.6.3.

## 8.7 En-values with results revised after draft A and draft B.1 report

The Excel spreadsheet *EURAMET.L-K8.2013-revised values.xlsx* contains values revised for BEV, NMISA and IPQ, according to section 8.5.1, 8.5.2, 8.5.3, 8.6.2 and 8.6.3. The En-values for the parameters subject to changes were calculated again and are summarized in Table 6. Values in red or their uncertainties were changed.

It has to be noted, that this analysis is in fact outside the scope of the key comparison, since the rules for CIPM MRA comparisons do not allow to change any results after draft A report. Therefore the key comparison reference values and the degrees of equivalence resulting from this comparison are those reported in the tables of section 8.2, the  $E_n$  values those of Table 5 in section 8.3. The partly substantial changes of the values from BEV and NMISA for the type A2 standard have an influence on the reference values and thus also to the  $E_n$  values of the other laboratories. These changes are certainly justified, since the original values refer to the wrong measurand, and one might argue, that the reference values after these changes are more reliable. For this reason, it is worthwhile to show the impact of the revised results on the  $E_n$  values, although, as stated above, outside the scope of the key comparison.

**Table 6.**  $E_n$  values of the revised results.

Institute	Type A2, KNT 2060/01, S/N 0589606						Type C1, PGN 10, no 682060 5				
	R1, d	R2, d	R3, d	R4, d	R5, d	R6, d	Ra	Rq	Rz	Rt	RSm
METAS	0.07	0.28	0.16	0.23	0.05	0.16	0.18	0.18	0.28	0.18	0.19
DTU-CGM	0.16	0.22	0.22	0.39	0.23	0.40	0.50	0.38	0.49	0.55	0.07
MIKES	0.15	0.20	0.18	0.09	0.04	0.01	0.07	0.13	0.19	0.29	1.10
IPQ	0.09	0.14	0.64	0.45	0.38	0.79	0.07	0.05	0.63	0.49	0.98
BEV	0.86	0.43	0.92	0.35	0.24	0.53	0.50	0.54	1.04	1.23	0.03
SP	0.31	0.07	0.03	0.10	0.03	0.16	0.27	0.29	0.52	0.42	0.17
INRIM	0.21	0.01	0.14	0.13	0.24	0.10	0.07	0.07	0.13	0.11	0.02
LNE	0.21	0.12	0.18	0.13	0.00	0.00	0.31	0.29	0.56	0.48	0.75
CEM	0.18	0.31	0.22	0.01	0.54	0.34	0.02	0.08	0.05	0.06	0.09
GUM	0.28	0.21	0.52	0.03	0.41	0.18	0.75	0.81	0.48	0.22	0.16
DMDM	0.57	0.43	0.24	0.02	0.10	0.05	0.19	0.15	0.12	0.13	0.00
UME	0.19	0.25	0.09	0.08	0.04	0.01	0.12	0.17	0.14	0.12	0.18
NIMT	0.23	0.17	0.59	0.63	0.70	0.61	0.26	0.23	0.01	0.00	0.05
NMC/A*STAR	0.01	0.14	0.04	0.07	0.24	0.22	0.22	0.23	0.43	0.39	0.03
CMS/ITRI	0.39	0.45	0.47	0.38	0.26	0.13	0.02	0.04	0.06	0.05	1.94
NMISA	0.34	0.24	0.14	0.04	0.09	0.00	0.20	0.19	0.25	0.23	0.00
INMETRO	0.23	0.05	0.00	0.36	0.34	0.07	0.07	0.02	0.03	0.05	0.32

Institute	Type D1, S/N 021				Type D1, KNT 2070/03, S/N 0986				Type C1, NIST SRM 2072, S/N 1015				
	Ra	Rq	Rz	Rt	Ra	Rq	Rz	Rt	Ra	Rq	Rz	Rt	RSm
METAS	0.72	0.70	0.60	0.67	0.01	0.09	0.03	0.04	0.04	0.07	0.02	0.06	0.23
DTU-CGM	1.95	2.05	1.61	0.24	0.12	0.16	0.19	0.12	0.13	0.06	0.74	0.74	0.04
MIKES	0.41	0.34	0.29	0.60	0.13	0.16	0.76	0.54	0.24	0.24	0.20	0.29	1.24
IPQ	0.19	0.23	0.18	0.07	0.00	0.07	0.05	0.06	0.13	0.12	0.06	0.01	0.74
BEV													
SP	0.05	0.19	0.24	0.11	0.01	0.01	0.31	0.61	0.16	0.11	1.71	1.98	0.91
INRIM	0.22	0.16	0.41	0.21	0.00	0.03	0.05	0.28	0.13	0.19	0.53	0.76	0.22
LNE	1.13	1.27	0.87	0.93	0.01	0.04	0.21	0.26	0.01	0.03	0.83	0.94	0.47
CEM	0.75	0.76	0.23	0.34	0.17	0.23	0.26	0.27	0.11	0.17	0.18	0.15	0.08
GUM	1.04	1.17	0.71	0.66	0.06	0.08	0.32	0.77	0.17	0.18	0.44	0.48	0.11
DMDM	0.43	0.31	0.02	0.30	0.10	0.17	0.31	0.21	0.22	0.21	0.18	0.18	0.06
UME	1.13	0.87	0.25	0.12	0.11	0.16	0.04	0.04	0.01	0.02	0.34	0.53	0.21
NIMT	0.53	0.66	0.82	0.55	0.00	0.08	0.05	0.01	0.38	0.79	0.46	0.16	0.06
NMC/A*STAR	0.69	0.79	1.42	1.63	0.00	0.08	0.07	0.21	0.04	0.07	0.35	0.31	0.07
CMS/ITRI	1.97	1.87	0.96	0.74	0.01	0.10	0.15	0.01	0.20	0.16	0.54	0.00	0.22
NMISA	0.82	0.93	1.01	0.95	0.18	0.21	0.32	0.13	0.00	0.01	0.01	0.03	0.01
INMETRO	0.24	0.18	0.58	0.38	0.08	0.11	0.43	0.16	0.00	0.02	0.12	0.23	0.36

## 8.8 Linking of result to other comparisons

The comparison followed the protocol of the former comparison EURAMET.L-K8.2009 as closely as possible. Also in the comparison APMP.L-K8.2008 similar artefacts were used. To what extent the three comparisons can be linked to each other, and whether this brings any added value, needs to be investigated by the CCL Task Group on comparison linking (TG-L) once the final reports of all three comparisons are available.



## 9 Softgauges

### 9.1 Description of the files

Two softgauges with type F1 reference data were sent to the participants. The files *METAS\_Aperiodic* and *METAS\_Periodic* were available in \*.smd and \*.prf format, the former according to ISO 5436-2, the latter to be compatible with Taylor Hobson Ultra software. The conditions for evaluation and the parameters to be determined are described in sections 4.6 and 5.4.

The aperiodic softgauge was produced from a measurement on a fine aperiodic roughness standard. The periodic softgauge was numerically generated from the superposition of two periodic waves with 100  $\mu\text{m}$  and 800  $\mu\text{m}$  wavelength and 100 nm and 20 nm amplitude, respectively, and adding some random noise with 5 nm amplitude.

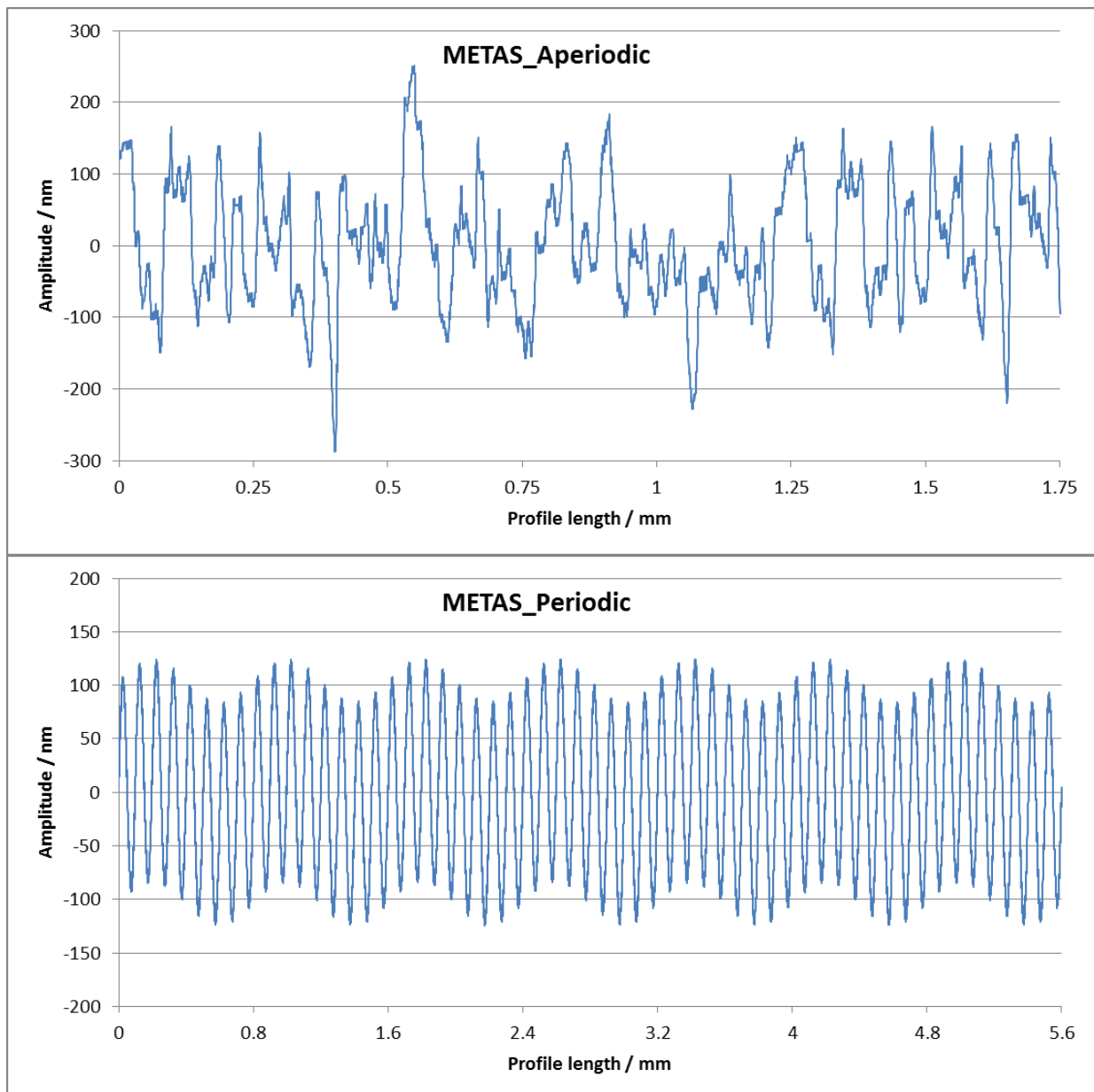


Figure 9. Profiles of the two softgauges.

## 9.2 Results of participants

**Table 7.** Results reported for METAS\_Periodic.smd with mean and standard deviation (UME excluded from mean and standard deviation).

	Ra (µm)	Rq (µm)	Rz (µm)	Rt (µm)	RSm (µm)
<b>METAS</b>	0.06376	0.071	0.2217	0.2234	99.815
<b>DTU_1</b>	0.064	0.071	0.221	0.226	100.0
<b>DTU_2</b>	0.064	0.071	0.222	0.223	100.0
<b>MIKES</b>	0.0637	0.071	0.2218	0.2235	100
<b>SP</b>	0.0638	0.071	0.2216	0.2234	100
<b>LNE</b>	0.06376512	0.07100243	0.22161773	0.2232598	100.092183
<b>INRIM_1</b>	0.0638	0.071	0.2217	0.2234	99.91
<b>INRIM_2</b>	0.0638	0.071	0.2217	0.2234	99.96
<b>UME</b>	0.064	0.071	0.229	0.229	100.061
<b>NIMT</b>	0.0638	0.071	0.2217	0.2234	-
<b>CEM</b>	0.063765	0.071002	0.221618	0.22326	100.092
<b>NMC/A*STAR</b>	0.0637	0.071	0.2218	0.2235	100
<b>CMS</b>	0.063767	0.071004	0.221688	0.223412	99.871429
<b>INMETRO</b>	0.0638	0.071	0.2216	0.2234	100.2837
<b>Mean</b>	0.063804	0.071001	0.22166	0.22356	100.002
<b>StdDev</b>	0.000093	0.000001	0.00023	0.00074	0.120

**Table 8.** Results reported for METAS\_Aperiodic.smd with mean and standard deviation (UME excluded from mean and standard deviation).

	Ra (µm)	Rq (µm)	Rz (µm)	Rt (µm)	Rsk
<b>METAS</b>	0.059883	0.074573	0.327789	0.456508	-0.033
<b>DTU_1</b>	0.06	0.075	0.328	0.457	-0.022
<b>DTU_2</b>	0.060	0.075	0.328	0.456	-0.033
<b>MIKES</b>	0.0595	0.0742	0.3276	0.4561	-0.0167
<b>SP</b>	0.0597	0.0744	0.3274	0.456	-0.0188
<b>LNE</b>	0.0598589	0.07393566	0.32751571	0.4563038	-0.141065
<b>INRIM_1</b>	0.0597	0.0744	0.3274	0.4561	-0.0186
<b>INRIM_2</b>	0.0599	0.0746	0.3278	0.4564	-0.0334
<b>UME</b>	0.061	0.075	0.337	0.459	-0.029
<b>NIMT</b>	0.0599	0.074	0.3278	0.4565	-0.1641
<b>CEM</b>	0.059859	0.073936	0.327516	0.456304	-0.141
<b>NMC/A*STAR</b>	0.0595	0.0742	0.3276	0.4561	-0.0186
<b>CMS</b>	0.059979	0.073939	0.327796	0.455334	-0.135478
<b>INMETRO</b>	0.0597	0.0744	0.3274	0.4561	-0.0186
<b>Mean</b>	0.05981	0.07435	0.32766	0.45621	-0.061
<b>StdDev</b>	0.00017	0.00037	0.00022	0.00038	0.059

**Table 9.** Software used by participating laboratories for evaluating the softgauges.

Institute	Software
<b>METAS</b>	METAS developed LabView software
<b>DTU_1</b>	Home made RCS4G
<b>DTU_2</b>	RoughnessPro by Image Metrology
<b>MIKES</b>	Taylor Hobson Ultra, Version n° : 5.14.9.70
<b>SP</b>	Taylor Hobson Ultra, Version n°: 4.6.8

<b>LNE</b>	Mountains Premium, Version n° : 6.2.6845
<b>INRIM_1</b>	Taylor Hobson Ultra V5.1.14
<b>INRIM_2</b>	RoughnessPro by Image Metrology
<b>UME</b>	Mahr Perthometer Concept, Version 6.3
<b>NIMT</b>	home made
<b>CEM</b>	Mountains Map, Version n° : 6.0.0.5727
<b>NMC/A*STAR</b>	Taylor Hobson Ultra, Version n° : 5.21.9.36
<b>CMS</b>	CMS_Surf.exe, version 2.1.1
<b>INMETRO</b>	Taylor Hobson Ultra, Version n° : 5.23.12.97

### 9.3 Graphical representation of deviations from the mean

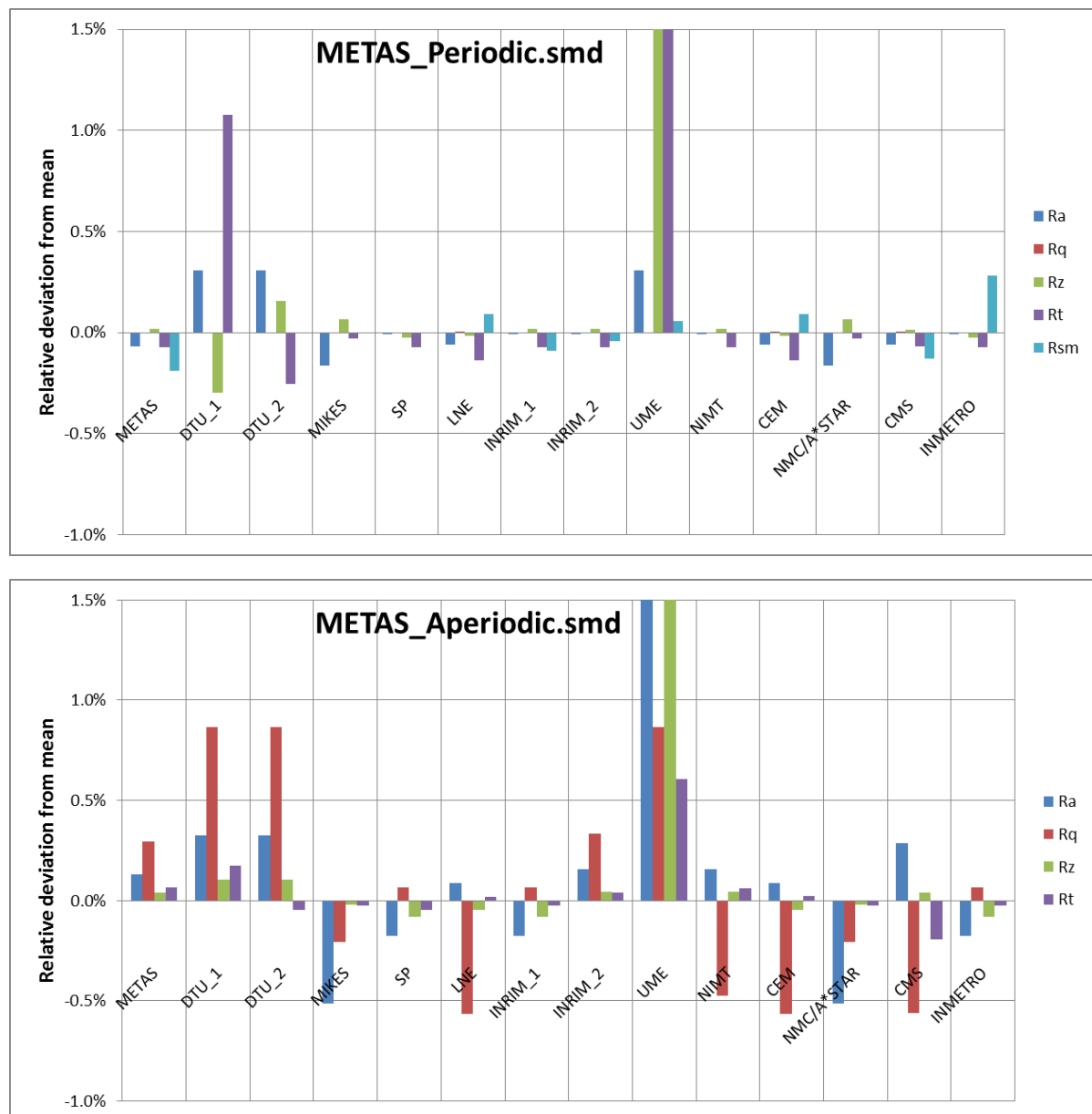


Figure 10. Relative deviation from mean.

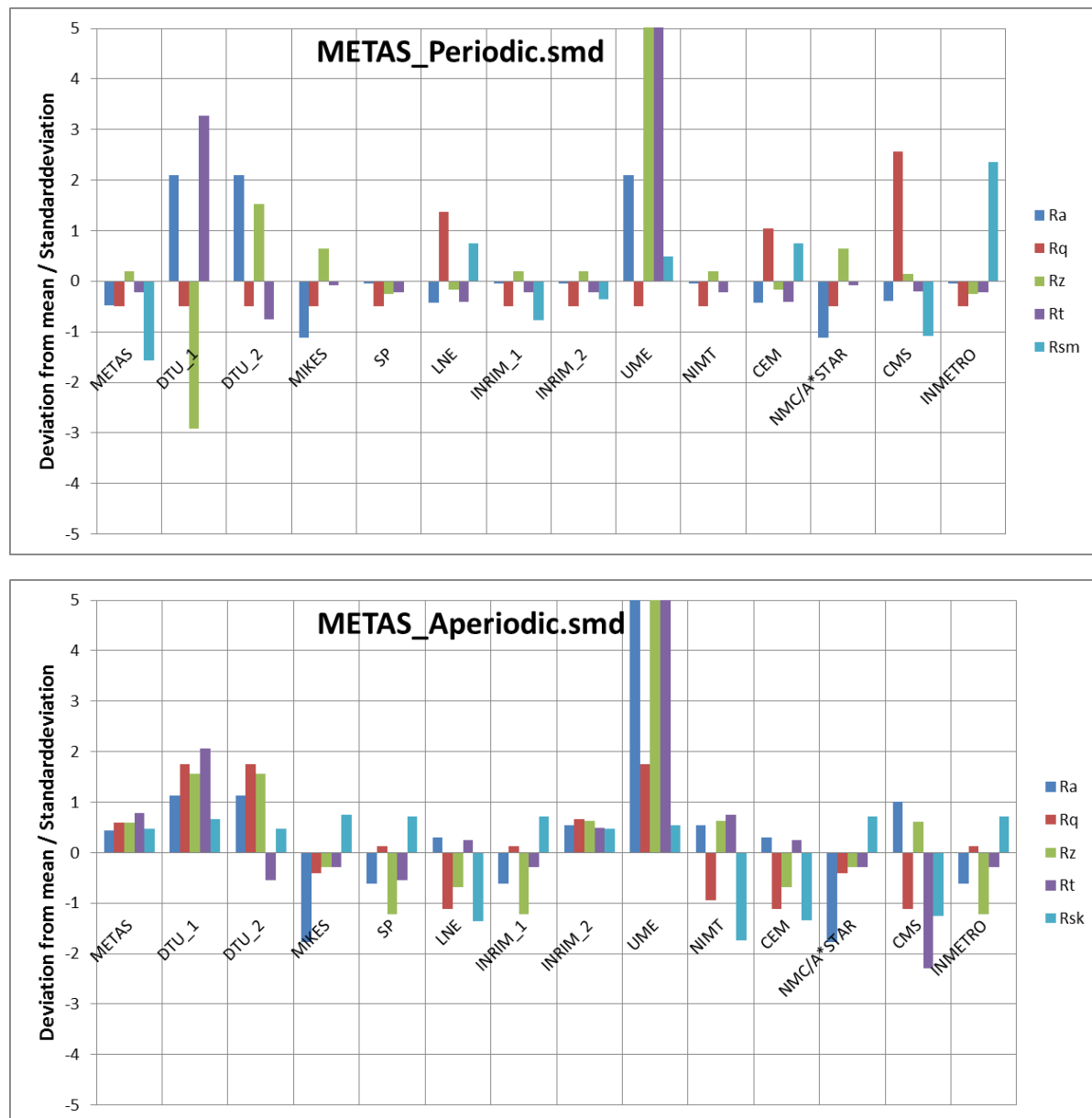


Figure 11. Deviation from mean in terms of multiples of the standard deviation.

## 10 Conclusions

After the first corrective actions and some corrections taken by a few of the participating laboratories, the number of  $E_n$  values  $> 1$  could be reduced from 32 to 20 out of a total of 395 individual results, which corresponds to 5 % and can statistically be expected, since the  $E_n$  criterion is based on a 95 % confidence interval. On good quality standards, such as the Halle A2 depth setting or the Halle D1 fine roughness standards, all results were in good agreement. 13 of the values with  $E_n > 1$  were observed on the Rubert D1 standard, which shows clear signs of use and damage and the largest standard deviations for the peak parameters, i.e. between 5 % and 10 %.

Regarding the softgauges, an analysis is much more difficult, since no uncertainties were quoted and reference values are not available (the mean of the reported results cannot be considered to be a reference value). Most of the results agree within roughly 0.2 % of the value. This can hardly be explained by numerical computation accuracy and a more detailed study needs to be carried out, taking into account the results of similar comparisons on other softgauges.

## 11 References

- [1] Calibration of surface roughness standards ,  
[http://kcdb.bipm.org/appendixB/KCDB\\_ApB\\_info.asp?cmp\\_idy=986&cmp\\_cod=EURAMET.L-K8&prov=exalead](http://kcdb.bipm.org/appendixB/KCDB_ApB_info.asp?cmp_idy=986&cmp_cod=EURAMET.L-K8&prov=exalead)
- [2] ISO 5436-1:2000, Geometrical Product Specifications (GPS) - Surface texture: Profile method; Measurement standards - Part 1: Material measures
- [3] ISO 4287:1997, Geometrical Product Specifications (GPS) - Surface texture: Profile method - Terms, definitions and surface texture parameters

## 12 Appendix: Equipment of the participating laboratories

Institute	Instrument	Stylus	Sampling spacing	Meas. speed	Meas. force
<b>METAS</b>	Taylor Hobson Talysurf FTS 120L	TH, 2 $\mu\text{m}$ , 90°	0.25 $\mu\text{m}$	0.5 mm / s	0.72 mN
<b>DTU-CGM</b>	Taylor Hobson Talysurf 5-120	TH, 2 $\mu\text{m}$ , 70°	0.1 $\mu\text{m}$	0.1 mm / s	-
<b>MIKES</b>	Taylor Hobson Form Talysurf	TH, 2 $\mu\text{m}$	0.25 $\mu\text{m}$	0.5 mm / s	1.2 mN
<b>IPQ</b>	Mahr Pethometer S8P	Mahr, 2 $\mu\text{m}$ , 90°	0.5 $\mu\text{m}$	0.5 mm / s	0.4 mN
<b>BEV</b>	SIOS NMM-1 with laser focus sensor (LFS)	SIOS LFS, integrated with NMM-1	0.1 $\mu\text{m}$	2 $\mu\text{m}$ / s	0 (optical)
<b>SP</b>	Taylor Hobson Form Talysurf 120	TH, 2 $\mu\text{m}$ , 90°	0.25 $\mu\text{m}$	0.5 mm / s	<0.70 mN
<b>INRIM</b>	Taylor Hobson Talystep 1	TH, 2.5 $\mu\text{m}$ , 90°	0.35 $\mu\text{m}$	25 $\mu\text{m}$ /s	40 .. 100 $\mu\text{m}$
	Taylor Hobson Form Talysurf II	TH, 2 $\mu\text{m}$ , 90°	0.25 $\mu\text{m}$	0.5 mm / s	1 mN
<b>LNE</b>	Homemade 3D profilometer with 3 laser interferometers	TH, 2 $\mu\text{m}$ , 90°	0.1 $\mu\text{m}$		<1 mN
<b>CEM</b>	KLA-Tencor P-6 Stylus Profiler	KLA-Tencor, 2 $\mu\text{m}$ , 60°	0.1 .. 0.2 $\mu\text{m}$	20 .. 200 $\mu\text{m}$ / s	0.02 .. 0.1 mN
<b>GUM</b>	Taylor Hobson Form Talysurf II	TH, 2 $\mu\text{m}$	0.25 $\mu\text{m}$	0.5 mm / s	0.7 mN
<b>DMDM</b>	Mahr MarSurf UD 120	Mahr, 2 $\mu\text{m}$ , 60°	0.25 $\mu\text{m}$	0.1 mm / s	0.7 mN
<b>UME</b>	Mahr Perthometer Concept	Mahr, 2 $\mu\text{m}$ , 90°	0.04 .. 0.5 $\mu\text{m}$	0.1 .. 0.5 mm / s	0.7 mN
<b>NIMT</b>	Kosaka ET 4000	Kosaka, 2 $\mu\text{m}$ , 60°	0.5 $\mu\text{m}$	0.05 mm / s	0.4 mN
<b>NMC/A*STAR</b>	Taylor Hobson PGI 2540	TH, 2 $\mu\text{m}$ , 60°	0.125 $\mu\text{m}$	0.1 .. 0.25 mm / s	0.75 mN
<b>CMS/ITRI</b>	Kosaka ET-4100 SURFCORDER	Kosaka, 2 $\mu\text{m}$ , 60°	0.025 .. 0.35 $\mu\text{m}$	0.02 .. 0.1 mm / s	0.05 mN
<b>NMISA</b>	Taylor Hobson Form Talysurf PGI 840	TH, 2 $\mu\text{m}$ , 60°	0.125 $\mu\text{m}$	1 mm / s	1 mN
<b>INMETRO</b>	Taylor Hobson PGI 830	TH, 2 $\mu\text{m}$ , 90°	0.125 $\mu\text{m}$	0.25 mm / s	1 mN

### 13 Appendix: Traceability of the participating laboratories

Institute	Vertical measurement traceability	NMI	Transverse measurement traceability	NMI
<b>METAS</b>	Reference sphere	METAS	Glass line scale artifact	METAS
<b>DTU-CGM</b>	6 step Halle standard	PTB	reference grid	NPL
<b>MIKES</b>	Calibration ball	MIKES	Type C1 Normals, calibrated with metrol. AFM	MIKES
<b>IPQ</b>	Surface texture standard type A1	CEM	Surface texture standard type D	IPQ
<b>BEV</b>	Laser interferometer	BEV	Laser interferometer	BEV
<b>SP</b>	Gauge blocks	SP	Invar line scale	SP
<b>INRIM</b>	Talystep 1: Precision displacement actuator Formtalsurf: precision ceramic ball	INRIM	stage micrometer and/or gratings	INRIM
<b>LNE</b>	Laser interferometer	LNE	Laser interferometer	LNE
<b>CEM</b>	Step height standards, calibrated by laser interferometer (on the NMM SIOS)	CEM	Line scale and grids, calibrated by laser interferometer (on the NMM SIOS)	CEM
<b>GUM</b>	Halle, type A2	PTB	Roughness standards type A2	PTB
<b>DMDM</b>	Roughness standard	HMI/FSB	Laser interferometer	DMDM
<b>UME</b>	Piezo transducer's actuator	UME	Type C standard PGN-3, calibrated by laser interferometer	UME
<b>NIMT</b>	Type A1 standard calibrated by laser interference microscope	NIMT	Standard glass scale calibrated by line scale interferometer	NIMT
<b>NMC/A*STAR</b>	Hemisphere	NMC/A*STAR	Hemisphere	NMC/A*STAR
<b>CMS/ITRI</b>	Step height standard	CMS/ITRI	Line scale standard	CMS/ITRI
<b>NMISA</b>	Reference sphere	NMISA	Reference sphere	NMISA
<b>INMETRO</b>	6 step height Halle	PTB	Line scale standard	INMETRO

## 14 Appendix: CMCs as declared by the participating laboratories in the CIPM MRA

CCL service categories related to surface texture:

- 5.1.1 (groove) depth (step height) standard (e.g. ISO 5436-1 Type A).
- 5.1.2 tip-condition standard (e.g. ISO 5436-1 Type B).
- 5.1.3 spacing standard (e.g. ISO 5436-1 Type C).
- 5.1.4 roughness standard (e.g. ISO 5436-1 Type D).
- 5.1.5 profile coordinate standard (e.g. ISO 5436-1 Type E).
- 5.1.6 softgauge standard (reference software data set).

NMI Service Id	CCL service category	Parameters	Range		$U(k = 2)$ (nm)	Remarks
			Min.	Max.		
METAS#44	5.1.1	$d$	0.1 $\mu\text{m}$	1000 $\mu\text{m}$	$Q[10, 0.2 d]$ , $d$ in $\mu\text{m}$	-
METAS#46	5.1.3	$Ra, Rq$	0.01 $\mu\text{m}$	100 $\mu\text{m}$	$Q[4, 16 Ra]$ , $Ra$ in $\mu\text{m}$	-
		$Rp, Rv, Rz, Rt$			$Q[30, 40 Rp]$ , $Rp$ in $\mu\text{m}$	-
METAS#47	5.1.4	$Ra, Rq$	0.01 $\mu\text{m}$	20 $\mu\text{m}$	$Q[4, 30 Ra]$ , $Ra$ in $\mu\text{m}$	-
		$Rp, Rv, Rz, Rt$			$Q[30, 60 Rp]$ , $Rp$ in $\mu\text{m}$	-
DTU/CGM	-	-	-	-	-	-
MIKES#41	5.1.1	$S$	0 $\mu\text{m}$	400 $\mu\text{m}$	$Q[10, 70 S]$ , $S$ in $\mu\text{m}$	
MIKES#42	5.1.3 5.1.4	$S$	0 $\mu\text{m}$	400 $\mu\text{m}$	$Q[10, 70 S]$ , $S$ in $\mu\text{m}$	
IPQ#101.40	5.1.3	$Ra$	0.1 $\mu\text{m}$	10 $\mu\text{m}$	$Q[50, 30 Ra]$ , $Ra$ in $\mu\text{m}$	-
		$Rz, Rp, Rv, Rt$			$Q[50, 30 Rz]$ , $Rz$ in $\mu\text{m}$	-
IPQ#101.40	5.1.4	$Ra$	0.1 $\mu\text{m}$	20 $\mu\text{m}$	$Q[50, 30 Ra]$ , $Ra$ in $\mu\text{m}$	-
		$Rz, Rp, Rv, Rt$			$Q[50, 30 Rz]$ , $Rz$ in $\mu\text{m}$	-
BEV#25	5.1.1	$d$	0.01 $\mu\text{m}$	10 $\mu\text{m}$	$Q[5, 10 d]$ , $d$ in $\mu\text{m}$	different technique
SP#36	5.1.1	$H$	0.05 $\mu\text{m}$	1000 $\mu\text{m}$	$Q[5, 20 H]$ , $H$ in $\mu\text{m}$	-
SP#37	5.1.3	$Ra, Rq$	0.01 $\mu\text{m}$	20 $\mu\text{m}$	$Q[5, 20 Ra]$ , $Ra$ in $\mu\text{m}$	-
		$Rz, Rt$			$Q[10, 30 Rz]$ , $Rz$ in $\mu\text{m}$	-



NMI Service Id	CCL service category	Parameters	Range		$U(k = 2)$ (nm)	Remarks
			Min.	Max.		
INRIM#24	5.1.1	$d$	0.01 $\mu\text{m}$	15 $\mu\text{m}$	$Q[1, 4.7 d]$ , $d$ in $\mu\text{m}$	
INRIM#33	5.1.3	$Ra$	0.1 $\mu\text{m}$	20 $\mu\text{m}$	$Q[10, 30 Ra]$ , $Ra$ in $\mu\text{m}$	-
		$Rz, Rp, Rv, Rt$			$Q[20, 50 Rz]$ , $Rz$ in $\mu\text{m}$	-
		$RSm$	50 $\mu\text{m}$	500 $\mu\text{m}$	0.5 $\mu\text{m}$	
INRIM#34	5.1.4	$Ra$	0.1 $\mu\text{m}$	20 $\mu\text{m}$	$Q[10, 30 Ra]$ , $Ra$ in $\mu\text{m}$	-
		$Rz, Rp, Rv, Rt$			$Q[20, 50 Rz]$ , $Rz$ in $\mu\text{m}$	-
LNE	-	-	-	-	-	-
CEM#33b	5.1.1	$H$	0.01 $\mu\text{m}$	15 $\mu\text{m}$	$Q[2, 20 H]$ , $H$ in $\mu\text{m}$	-
CEM#34	5.1.4	$Ra$	0.01 $\mu\text{m}$	15 $\mu\text{m}$	$Q[9, 30 Ra]$ , $Ra$ in $\mu\text{m}$	-
		$Rz$			$Q[14, 40 Rz]$ , $Rz$ in $\mu\text{m}$	-
GUM#26	5.1.1	$Pt, d$	0.1 $\mu\text{m}$	100 $\mu\text{m}$	$Q[30, 0.5 d]$ , $d$ in $\mu\text{m}$	-
GUM#27	5.1.3	$Ra, Rq$	0.05 $\mu\text{m}$	30 $\mu\text{m}$	$Q[15, 25 Ra]$ , $Ra$ in $\mu\text{m}$	-
		$Rz, Rt$			$Q[40, 50 Rp]$ , $Rp$ in $\mu\text{m}$	-
GUM#28	5.1.4	$Ra, Rq$	0.05 $\mu\text{m}$	30 $\mu\text{m}$	$Q[15, 30 Ra]$ , $Ra$ in $\mu\text{m}$	-
		$Rz, Rt$			$Q[40, 60 Rp]$ , $Rp$ in $\mu\text{m}$	-
DMDM	-	-	-	-	-	-
UME#34	5.1.1	$d$	0.01 $\mu\text{m}$	750 $\mu\text{m}$	$Q[18, 30 d]$ , $d$ in $\mu\text{m}$	-
UME#35	5.1.3	$Ra, Rq, Rz, Rp, Rt, Rv$	0.01 $\mu\text{m}$	20 $\mu\text{m}$	$Q[10, 40 Ra]$ , $Ra$ in $\mu\text{m}$	-
UME#36	5.1.4	$Ra, Rq, Rz, Rp, Rt, Rv, Rpk, Rvk, Mr_1, Mr_2$	0.01 $\mu\text{m}$	20 $\mu\text{m}$	$Q[10, 40 Rz]$ , $Rz$ in $\mu\text{m}$	-
NIMT#08060-10501	5.1.1	$d$	25 nm	32 $\mu\text{m}$	$Q[6.6, 12 d]$ , $d$ in $\mu\text{m}$	-
NIMT#08060-10601	5.1.3	$Ra$	25 nm	32 $\mu\text{m}$	$Q[10, 12 Ra]$ , $Ra$ in $\mu\text{m}$	-
	5.1.4	$Rz$			$Q[18, 17 Rz]$ , $Rz$ in $\mu\text{m}$	-
NMC/A*STAR #D049	5.1.4	ISO roughness parameters (eg. $Ra$ )	0.1 $\mu\text{m}$	10 $\mu\text{m}$	$Q[36, 30 Ra]$ , $Ra$ in $\mu\text{m}$	-

NMI Service Id	CCL service category	Parameters	Range		$U(k = 2)$ (nm)	Remarks
			Min.	Max.		
CMS#D21	5.1.1	$D$	0.01 $\mu\text{m}$	50 $\mu\text{m}$	$Q[5, 3.2 D]$ , $D$ in $\mu\text{m}$	
CMS#D13	5.1.3 5.1.4	$Ra, Rq$	0.01 $\mu\text{m}$	20 $\mu\text{m}$	$Q[5, 13 R]$ , $R$ in $\mu\text{m}$	
NMISA#	5.1.1	$d$	0.01 $\mu\text{m}$	3000 $\mu\text{m}$	$Q[4, 20 d]$ , $d$ in $\mu\text{m}$	
NMISA#	5.1.3 5.1.4	$Ra$	0.01 $\mu\text{m}$	100 $\mu\text{m}$	$Q[10, 30 Ra]$ , $Ra$ in $\mu\text{m}$	
INMETRO#27	5.1.1	$H$	0.05 $\mu\text{m}$	20 $\mu\text{m}$	$20 + 2 H$ , $H$ in $\mu\text{m}$	
INMETRO#29	5.1.3 5.1.4	$Ra, Rz, Rmax$	0.01 $\mu\text{m}$	20 $\mu\text{m}$	$10 + 20 Ra$ , $Ra$ in $\mu\text{m}$	